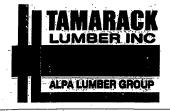


		Products		
PlotID	Length	Product	Plies	Net Qty
J1	16-00-00	9 1/2" NI-40x	1	7
J2	14-00-00	9 1/2" NI-40x	1	31
J3	12-00-00	9 1/2" NI-40x	1	7
J3DJ	12-00-00	9 1/2" NI-40x	2	4
J4	10-00-00	9 1/2" NI-40x	1	6
J5	6-00-00	9 1/2" NI-40x	1	1
J6	4-00-00	9 1/2" NI-40x	1	1
J7	2-00-00	9 1/2" NI-40x	1	4
B2	10-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2
B4	10-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2
B5	8-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	1	1
B1	8-00-00	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2
B3	00-00-8	1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP	2	2

(	Connector Summary								
Qty	Manuf	Product							
26	H1	IUS2.56/9.5							
2	H1	IUS2.56/9.5							
6	H1	IUS2.56/9:5							
1	H2	HUS1.81/10							
2	H3	HGUS410							



FROM PLAN DATED:

**BUILDER: GREENPARK HOMES** 

SITE: RUSSEL GARDENS

**MODEL:** HIGHGROVE 11

**ELEVATION: 2** 

LOT:

CITY: WATERDOWN

SALESMAN: M D DESIGNER: AJ REVISION:

NOTES:

REFER TO THE NORDIC **INSTALLATION** GUIDE FOR PROPER STORAGE AND INSTALLATION. **SQUASH BLOCKS** OF 2x4, 2x6, 2x8 #2 S.P.F REQ'D UNDER INTERIOR UNIFORM LOAD BEARING WALLS. MULTIPLE SQUASH BLOCKS REQ'D UNDER CONCENTRATED LOADS. SEE FIGURE 1. CANTILEVERED JOISTS INCLUDING CANT' OVER BRICK REQ. I-JOIST BLOCKING ALONG BEARING AND RIMBOARD CLOSURE AT ENDS. SEE FIGURES 4 & 5 FOR REINFORCEMENT REQUIREMENTS. FOR HOLES INCLUDING DUCT CHASE AND FIELD CUT OPENINGS SEE FIGURE 7. TABLES 1 & 2. **CERAMIC TILE APPLICATION AS PER** O.B.C 9.30.6. LOADING:

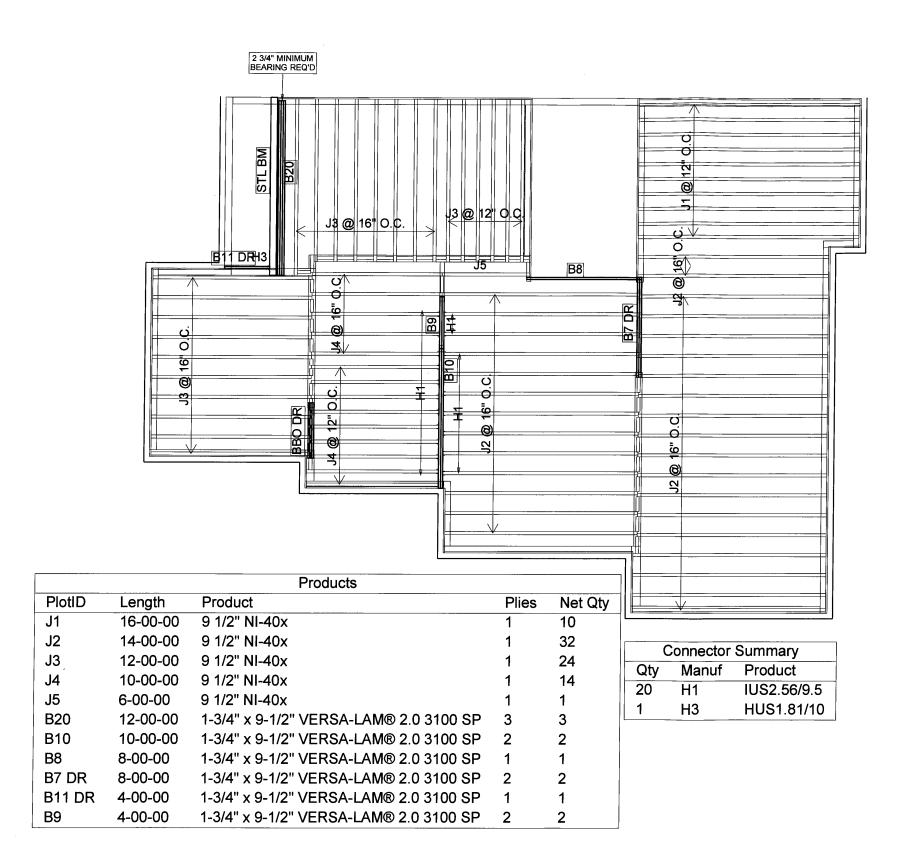
DESIGN LOADS: L/480.000 LIVE LOAD: 40.0 lb/ft² DEAD LOAD: 15.0 lb/ft

TILED AREAS: 20 lb/ft

SUBFLOOR: 3/4" GLUED AND NAILED

DATE: 6/7/2017

### 1st FLOOR





FROM PLAN DATED:

**BUILDER: GREENPARK HOMES** 

SITE: RUSSEL GARDENS

**MODEL: HIGHGROVE 11** 

**ELEVATION**: 2

LOT:

**CITY: WATERDOWN** 

SALESMAN: M D DESIGNER: AJ REVISION:

NOTES:

REFER TO THE NORDIC INSTALLATION **GUIDE FOR PROPER STORAGE AND** INSTALLATION. **SQUASH BLOCKS** OF 2x4, 2x6, 2x8 #2 S.P.F. REQ'D UNDER INTERIOR UNIFORM LOAD BEARING WALLS. MULTIPLE **SQUASH BLOCKS** REQ'D UNDER CONCENTRATED LOADS. SEE FIGURE 1. **CANTILEVERED JOISTS INCLUDING CANT'** OVER BRICK REQ. I-JOIST BLOCKING ALONG BEARING AND RIMBOARD CLOSURE AT ENDS. SEE FIGURE 7 TABLES 4 & 5 FOR REINFORCEMENT REQUIREMENTS. FOR HOLES INCLUDING DUCT CHASE AND FIELD **CUT OPENINGS** SEE FIGURE 7 TABLES 1 & 2 OF THE INSTALLATION GUIDE. CERAMIC TILE APPLICATION AS PER O.B.C. 9.30.6

LOADING:

DESIGN LOADS: L/480.000 LIVE LOAD: 40.0 lb/ft<sup>2</sup> DEAD LOAD: 15.0 lb/ft<sup>2</sup> TILED AREAS: 20 lb/ft<sup>2</sup>

**SUBFLOOR: 5/8" GLUED AND NAILED** 

**DATE:** 2018-02-20

### 2nd FLOOR



COMPANY TAMARACK LUMBER BURLINGTON Feb. 20, 2018 15:22 **PROJECT**J3 2ND FLR GARAGE

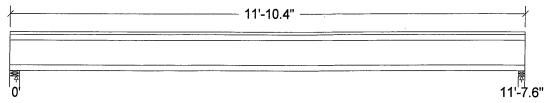
### **Design Check Calculation Sheet**

Nordic Sizer - Canada 6.4

### Loads:

Load	Туре	Distribution	Pat-	Location	[ft]	Magnitud	le	Unit
			tern	Start	End	Start	End	
Load1	Dead	Full Area				20.00		psf
Load2	Live	Full Area				40.00		psf

### Maximum Reactions (lbs), Bearing Resistances (lbs) and Bearing Lengths (in):



	U	11-7.0
Unfactored:	1	
Dead	159	157
Live	319	314
Factored:		
Total	677	668
Bearing:		
Resistance		
Joist	1871	1854
Support	4756	2758
Des ratio		
Joist	0.36	0.36
Support	0.14	0.24
Load case	#2	#2
Length	2-3/4	1-3/4*
Min req'd	1-3/4	1-3/4
Stiffener	No	No
Kd	1.00	1.00
KB support	1.00	1.00
fcp sup	769	769
Kzcp sup	1.13	1.02

\*Minimum bearing length for joists is 1-3/4" for exterior supports

Bearing for wall supports is perpendicular-to-grain bearing on top plate. No stud design included.

Nordic Joist 9-1/2" NI-40x Floor joist @ 16" o.c.

Supports: All - Lumber Wall, No.1/No.2

Total length: 11'-10.4"; 5/8" nailed and glued OSB sheathing

This section PASSES the design code check.



DWG NO. TAM 9653 - R STRUCTURAL COMPONENT ONLY

### WoodWorks® Sizer

### for NORDIC STRUCTURES

### **J3 2ND FLR GARAGE**

### Nordic Sizer - Canada 6.4

Page 2

### Limit States Design using CSA 086-14 and Vibration Criterion:

Criterion	Analysis Value	Design Value	Unit	Analysis/Design
Shear	Vf = 659	Vr = 1895	lbs	Vf/Vr = 0.35
Moment(+)	Mf = 1919	Mr = 4824	lbs-ft	Mf/Mr = 0.40
Perm. Defl'n	$0.05 = \langle L/999 \rangle$	0.39 = L/360	in	0.13
Live Defl'n	$0.10 = \langle L/999$	0.29 = L/480	in	0.34
Total Defl'n	0.15 = L/933	0.58 = L/240	in	0.26
Bare Defl'n	$0.12 = \langle L/999 \rangle$	0.39 = L/360	in	0.31
Vibration	Lmax = 11'-8	Lv = 15'-4	ft	
Defl'n	= 0.025	= 0.061	in	0.41

### **Additional Data:**

FACTORS:	f/E	KD	KH	KZ	KL	KT	KS	KN	LC#
Vr	1895	1.00	1.00	-	_	-	-	_	#2
Mr+	4824	1.00	1.00	-	1.000	_	-	_	#2
ΕI	218.1 m	illion	_	_	_	_	_	_	#2

### **CRITICAL LOAD COMBINATIONS:**

Support 2 - LC #2 = 1.25D + 1.5L Load Types: D=dead W=wind S=snow H=earth,groundwater E=earthquake

L=live(use, occupancy) Ls=live(storage, equipment) f=fire

Load Patterns: s=S/2 L=L+Ls \_=no pattern load in this span All Load Combinations (LCs) are listed in the Analysis output

### CALCULATIONS:

Deflection: EIeff = 268e06 lb-in2 K= 4.94e06 lbs "Live" deflection = Deflection from all non-dead loads (live, wind, snow...)

### **Design Notes:**

- 1. WoodWorks analysis and design are in accordance with the 2010 National Building Code of Canada (NBC Part 4) and the CSA O86-14 Engineering Design in Wood standard (May 2014 edition). CONFORM\$ TO OBC 2012
- 2. Please verify that the default deflection limits are appropriate for your application.
- 3. Refer to technical documentation for installation guidelines and construction details.
- 4. Nordic I-joists are listed in CCMC evaluation report 13032-R.
- 5. Joists shall be laterally supported at supports and continuously along the compression edge.
- 6. The design assumptions and specifications have been provided by the client. Any damages resulting from faulty or incorrect information, specifications, and/or designs furnished, and the correctness or accuracy of this information is their responsibility. This analysis does not constitute a record of the structural integrity of the building nor suitability of the design assumptions made. Nordic Structures is responsible only for the structural adequacy of this component based on the design criteria and loadings shown.

S. KATSOULAKOS E

DWG NO. TAM 9653-18 STRUCTURAL COMPONENT ONLY



### Boise Cascade Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP Basment\Flush Beams\B1(i1294)

BC CALC® Design Report

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:11

Build 5033

Job Name:

Address:

City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Flush Beams\Basment\Flush Beams\B1(i1294)

Specifier:

Designer: Company:

Misc:

3/		\\ \frac{\dagger}{\psi} \\ \frac{\dagger}{\psi} \\ \frac{\dagger}{\dagger}
	07-03-06	<b>⊠</b>

Total Horizontal Product Length = 07-03-06

Reaction Summary (Down / Uplift) (Ibs)						
Bearing	Live	De ad	Snow	Wind		
B0, 7-1/4"	4,010/0	2,125 / 0				
B1, 6-3/4"	4,582 / 0	2,442/0				

Lo	ad Summary					Live	Dead	Snow	Wind	Trib.
Tag Description		Load Type Ref. Start End 1.0		1.00	0.65	1.00	1.15			
0	7(i350)	Unf. Lin. (lb/ft)	L	00-00-00	00-07-10		81			n/a
1	Smoothed Load	Unf. Lin. (lb/ft)	L	01-02-02	05-02-02	521	261			n/a
2	8(i365)	Unf. Lin. (lb/ft)	L	06-08-04	07-03-06	264	212			n/a
3	- '	Conc. Pt. (lbs)	L	00-06-08	00-06-08	2,707	1,386			n/a
4	-	Conc. Pt. (lbs)	L	05-10-02	05-10-02	656	329			n/a
5	_	Conc. Pt. (lbs)	L	06-09-14	06-09-14	2.979	1.557			n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	5,431 ft-lbs	25,408 ft-lbs	21.4%	1	03-02-02
End Shear	3,105 lbs	11,571 lbs	26.8%	1	05-11-02
Total Load Defl.	L/999 (0.053")	n/a	n/a	4	03-08-02
Live Load Defl.	L/999 (0.035")	n/a	n/a	5	03-08-02
Max Defl.	0.053"	n/a	n/a	4	03-08-02
Span / Depth	7.9	n/a	n/a		00-00-00

				De mand/ Resistance	Demand/ Resistance	
Bea	ring Supports	Dim.(LxW)	Demand	Support	Member	Material
B0	Beam	7-1/4" x 3-1/2"	8,672 lbs	80%	28%	Unspecified
B1	Wall/Plate	6-3/4" x 3-1/2"	9,925 lbs	98.3%	34.4%	Unspecified

### Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

CONFORMS TO UBG 2012

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9



DWO NO. TAM YOUT - 17
STRUCTURAL
COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP Basment\Flush Beams\B1(i1294)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:11

BC CALC® Design Report

\*

Build 5033

Job Name: Address:

City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

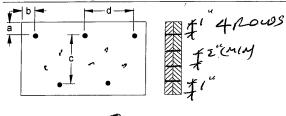
Description: Designs\Flush Beams\Basment\Flush Beams\B1(i129

Specifier: Designer:

Company.

Misc:

### **Connection Diagram**



Calculated Side Load = 779.8 lb/ft

Connection design assumes point load is top-loaded. For connection design of side-loaded point loads, please consult a technical representative or professional of Record.

Connectors are: 16d Nails 3½" ARDOX SPIRAL

### Disclosure

Completeness and accuracy of input must be verified by anyone w ho w ould rely on output as evidence of suitability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered w ood products must be in accordance w ith current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

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DWO NO .TAM 47641 -17 STRUCTURAL COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP Basment\Flush Beams\B3(i1322)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:12

BC CALC® Design Report

Build 5033

Job Name: Address:

City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Flush Beams\Basment\Flush Beams\B3(i1322)

Specifier: Designer: Company:

Misc:

<b>1</b> /	2	3	4	5
	1 1 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
				/
<b>B</b> 0		06-02-10		B1

Total Horizontal Product Length = 06-02-10

Reaction Summary (Down / Uplift) ( lbs )								
Be aring	Live	De ad	Snow	Wind				
B0, 2-3/8"	1,242 / 0	650/0						
B1 <sup>'</sup>	1,445 / 0	751/0						

1.0	ad Summary					Live	Dead	Snow	Wind	Trib.
Tag Description		Load Type	Ref. Start	En d	1.00	0.65	1.00	1.15		
0	Smoothed Load	Unf. Lin. (lb/ft)	L	00-02-14	04-02-14	265	132			n/a
1	J5(i929)	Conc. Pt. (lbs)	L	00-10-14	00-10-14	208	104			n/a
2	J5(i923)	Conc. Pt. (lbs)	L	02-02-14	02-02-14	231	115			n/a
3	J5(i379)	Conc. Pt. (lbs)	L	03-06-14	03-06-14	231	115			n/a
4	-	Conc. Pt. (lbs)	L	04-10-14	04-10-14	586	293			n/a
5	J2(i1301)	Conc. Pt. (lbs)	L	06-01-06	06-01-06	355	177			n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	4,244 ft-lbs	25,408 ft-lbs	16.7%	1	03-06-14
End Shear	2,535 lbs	11,571 lbs	21.9%	1	00-11-14
Total Load Defl.	L/999 (0.038")	n/a	n/a	4	03-01-14
Live Load Defl.	L/999 (0.025")	n/a	n/a	5	03-01-14
Max Defl.	0.038"	n/a	n/a	4	03-01-14
Span / Depth	7.6	n/a	n/a		00-00-00

				Resistance	Resistance	
Bea	ring Supports	Dim.(L x W)	Demand	Support	Member	Material
B0	Wall/Plate	2-3/8" x 3-1/2"	2,676 lbs	75.3%	26.4%	Unspecified
B1	Hanger	2" x 3-1/2"	3,106 lbs	n/a	36.4%	Hanger

### Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA CONFORMS TO OBC 2012

086.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9



DWO NO . TAM 47642 17 STRUCTURAL COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP Basment\Flush Beams\B3(i1322)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:12

BC CALC® Design Report

Build 5033 Job Name:

Address: City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

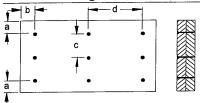
Description: Designs\Flush Beams\Basment\Flush Beams\B3(i132)

Specifier:

Designer: Company.

Misc:

Connection Diagram



a minimum = 2"

c = 2-3/4"

d = 🌌 b minimum = 3"

Calculated Side Load = 598.7 lb/ft

Connection design assumes point load is top-loaded. For connection design of side-loaded point loads, please consult a technical representative or professional of Record.

Connectors are: 16d 3000000 Nails

312" ARDOX SPIRAL

### Disclosure

Completeness and accuracy of input must be verified by anyone who would rely on output as evidence of suitability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

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DWG NO . TAM 4764217 STRUCTURAL COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP Basment\Flush Beams\B2(i1275)



Dry | 2 spans | Right cantilever | 0/12 slope (deg)

June 7, 2017 09:38:12

BC CALC® Design Report

**Build 5033** Job Name: Address:

City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

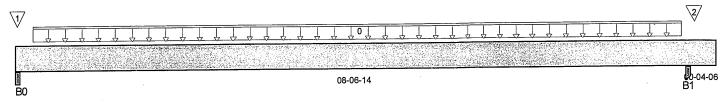
File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Flush Beams\Basment\Flush Beams\B2(i1275)

Specifier:

Designer: Company.

Misc:



Total Horizontal Product Length = 08-11-04

Reaction Summary (Down Bearing	/ Uplift) (lbs) Live	Dead	Snow	Wind	
B0, 2-5/8"	221/0	180/0			
B1, 5-1/4"	4,854/0	2,686/0			

Lood Cumama n				Live		Snow Wind	Trib.
Load Summary Tag Description	Load Type	Ref. Start	En d	1.00	0.65	1.00 1.15	
0 FC1 Floor Material	Unf. Lin. (lb/ft)	L 00-02-10	08-06-00	32	16		n/a
1 11(i372)	Conc. Pt. (lbs)	L 00-00-04	00-00-04	80	68		n/a
2 -	Conc. Pt. (lbs)	L 08-07-12	08-07-12	4,721	2,576 ♣	top eable leanen.	n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	710 ft-lbs	25,408 ft-lbs	2.8%	1	04-04-11
End Shear	269 lbs	11,571 lbs	2.3%	1	01-00-02
Cont. Shear	257 lbs	11,571 lbs	2.2%	1	07-06-12
Total Load Defl.	L/999 (0.013")	n/a	n/a	4	04-04-11
Live Load Defl.	L/999 (0.007")	n/a	n/a	5	04-04-11
Total Neg. Defl.	2xL/1.998 (-0.0	02") n/a	n/a	4	08-11-04
Max Defl.	0.013"	n/a	n/a	4	04-04-11
Span / Depth	10.6	n/a	n/a		00-00-00

<b>P</b> o aris	ng Supports	Dim.(L x W)	De man d	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Beam	2-5/8" x 3-1/2"	556 lbs	14.2%	5%	Unspecified
B1	Post	5-1/4" x 3-1/2"	10,638 lbs	89.1%	47.5%	Unspecified

### Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA CONFORMS TO OBC 2012 O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

Cantilevers require sheathed bottom flanges, blocking at cantilever support and clesure atends.



DWG NO . TAM 47643-17 STRUCTURAL COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP Basment\Flush Beams\B2(i1275)

BC CALC® Design Report



Dry | 2 spans | Right cantilever | 0/12 slope (deg)

June 7, 2017 09:38:12

**Build 5033** 

Job Name:

Address: City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Flush Beams\Basment\Flush Beams\B2(i127:

Specifier:

Designer: Company.

Misc:

### **Connection Diagram**

Concentrated side-load exceeds allowable magnitude for connection design. Please consult a technical representative or Professional Engineer for the design of the connection. OL 474

MALLING

PROVIDE FROWS OF 3½" ARDOX SPIRAL NAILS @ 12—" O/C FOR MULTI-PLY NAILING, MAINTAIN A MIN. L" LUMBER EDGE/END DISTANCE, DO NOT USE AIR NAILS

### Disclosure

Completeness and accuracy of input must be verified by anyone who would rely on output as evidence of suitability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered w ood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

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### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP Basment\Flush Beams\B4(i1306)

\*

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:12

BC CALC® Design Report

gn Report

Build 5033 Job Name: Address:

City, Province, Postal Code:,

Customer:

Code reports:

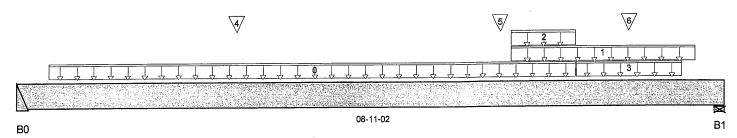
CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Flush Beams\Basment\Flush Beams\B4(i1306)

Specifier: Designer: Company.

Misc:



Total Horizontal Product Length = 08-11-02

 Reaction Summary (Down / Uplift) ( lbs )

 Bearing
 Live
 Dead
 Snow
 Wind

 B0
 3,335 / 0
 1,859 / 0

 B1, 4-3/8"
 2,875 / 0
 1,724 / 0

10	ad Summary					Live	Dead	Snow	Wind	i rib.
	g Description	Load Type	Re	f. Start	En d	1.00	0.65	1.00	1.15	
0	Smoothed Load	Unf. Lin. (lb/ft)	L	00-04-12	07-00-12	272	136			n/a
1	12(i481)	Unf. Lin. (lb/ft)	L	06-02-12	08-06-12		65			n/a
2	12(i481)	Unf. Lin. (lb/ft)	L	06-02-12	07-00-12	692	346			n/a
3	12(i481)	Unf. Lin. (lb/ft)	L	07-00-12	08-04-12	208	104			n/a
4	PBO4(i408)	Conc. Pt. (lbs)	L	02-09-00	02-09-00	2,798	1,541			n/a
5	PBO3(i407)	Conc. Pt. (lbs)	L	06-01-00	06-01-00	571	385			n/a
6	J6(i1183)	Conc. Pt. (lbs)	L	07-08-12	07-08-12	158	79			n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	17,679 ft-lbs	25,408 ft-lbs	69.6%	1	02-09-00
End Shear	7,301 lbs	11,571 lbs	63.1%	1	00-11-08
Total Load Defl.	L/321 (0.319")	0.426"	74.9%	4	04-02-12
Live Load Defl.	L/502 (0.204")	0.284"	71.7%	5	04-02-12
Max Defl.	0.319"	n/a	n/a	4	04-02-12
Span / Depth	10.8	n/a	n/a		00-00-00

				Demand/ Resistance	Resistance	
Bear	ring Supports	Dim.(LxW)	De man d	Support	Member	Material
B0	Hanger	2" x 3-1/2"	7,326 lbs	n/a	85.8%	Hanger
B1	Wall/Plate	4-3/8" x 3-1/2"	6,468 lbs	98.9%	34.6%	Unspecified

Notes



DWG NO. TAM 47644-17 STRUCTURAL COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP Basment\Flush Beams\B4(i1306)

BC CALC® Design Report



Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:12

Build 5033

Job Name:

Address:

City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs \Flush Beams \Basment\Flush Beams \B4(i130)

Specifier:

Designer: Company:

Misc:

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

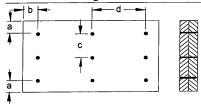
BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA CONFORMS TO OBC 2012

O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

### Connection Diagram



c = 2-3/4" a minimum = 2" b minimum = 3"

Calculated Side Load = 468.2 lb/ft

Connection design assumes point load is top-loaded. For connection design of side-loaded point loads, please consult a technical representative or professional of Record.

Connectors are: 16d ARDDX SPIRAL

### Disclosure

Completeness and accuracy of input must be verified by anyone who would rely on output as evidence of suitability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

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DWO NO. TAM 4764417 STRUCTURAL COMPONENT ONLY



### Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP Basment\Flush Beams\B5(i1282)

BC CALC® Design Report

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:12

Build 5033

Job Name:

Address:

City, Province, Postal Code:,

Customer:

Code reports:

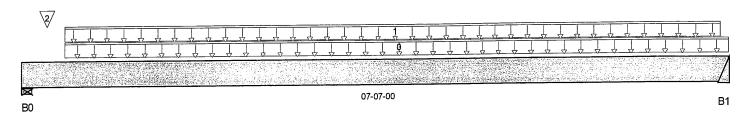
CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Flush Beams\Basment\Flush Beams\B5(i1282)

Specifier: Designer: Company.

Misc:



Total Horizontal Product Length = 07-07-00

			<del></del>	<del></del>					
Reaction Summary (Down / Uplift) (lbs)									
Be aring	Live	De ad	Snow	wind					
B0, 5-1/2"	1,154 / 0	617/0							
B1	948/0	491/0							

Land Common me				Live	Dead	Snow Wind	Trib.
Load Summary Tag Description	Load Type	Ref. Start	En d	1.00	0.65	1.00 1.15	
0 User Load	Unf. Lin. (lb/ft)	L 00-05-08	07-07-00	240	120		n/a
1 FC1 Floor Material	Unf. Lin. (lb/ft)	L 00-05-08	07-06-00	20	10		n/a
2 9(i368)	Conc. Pt. (lbs)	L 00-03-04	00-03-04	236	139		n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	3,508 ft-lbs	12,704 ft-lbs	27.6%	1	03-11-04
End Shear	1,504 lbs	5,785 lbs	26%	1	01-03-00
Total Load Defl.	L/999 (0.09")	n/a	n/a	4	03-11-04
Live Load Defl.	Ľ⁄999 (0.059'')	n/a	n/a	5	03-11-04
Max Defl.	0.09" `	n/a	n/a	4	03-11-04
Span / Depth	8.9	n/a	n/a		00-00-00

Rearin	ng Supports	Dim . (L x W)	Demand	De m an d/ Re s istance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	5-1/2" x 1-3/4"	2,503 lbs	60.9%	21.3%	Un specified
B1	Hanger	2" x 1-3/4"	2,036 lbs	n/a	47.7%	Hanger

### Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA O86.

CONFORMS TO OBC 2012

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

### Disclosure

Completeness and accuracy of input must be verified by anyone w ho w ould rely on output as evidence of suitability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered w ood products must be in accordance w ith current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

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DWO NO . TAM 47645-17 STRUCTURAL COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1st Floor\...\B7 DR(i1321)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:12

BC CALC® Design Report

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Dropped Beams\1st Floor\Dropped Beams\B7 D

Specifier:

Designer:

Misc:

Company.

City, Province, Postal Code:,

Customer:

**Build 5033** 

Job Name: Address:

Code reports:

CCMC 12472-R

06-08-10 В1 В0

Total Horizontal Product Length = 06-08-10

Reaction Summary (Down / Uplift) (lbs)							
Be aring	Live	De ad	Snow	Wind			
B0, 4"	2,005 / 0	1,034 / 0					
B1,4"	1,714/0	908/0					

١o	ad Summary					Live	Dead	Snow	Wind	Trib.
	g Description	Load Type	Re f.	Start	En d	1.00	0.65	1.00	1.15	
0	Smoothed Load	Unf. Lin. (lb/ft)	L (	00-00-00	04-10-08	564	281			n/a
1	-	Conc. Pt. (lbs)	L (	05-05-12	05-05-12	675	338			n/a
2	B8 (i1200)	Conc. Pt. (lbs)	L (	06-07-08	06-07-08	288	163			n/a

	Factored	Factored	Demand /	Load	Location
Controls Summary	Dem and	Resistance	Resistance	Case	
Pos. Moment	5,230 ft-lbs	25,408 ft-lbs	20.6%	1	02-10-08
End Shear	3,052 lbs	11,571 lbs	26.4%	1	05-07-02
Total Load Defl.	L/999 (0.051")	n/a	n/a	4	03-03-15
Live Load Defl.	L/999 (0.033'')	n/a	n/a	5	03-03-15
Max Defl.	0.051"	n/a	n/a	4	03-03-15
Span / Depth	7.8	n/a	n/a		00-00-00

Bear	ring Supports	Dim . (L x W)	Demand	De man d/ Re s istance Support	De mand/ Re s istance Me m be r	Material
B0	Wall/Plate	4" x3-1/2"	4,301 lbs	47.3%	25.2%	Unspecified
B1	Wall/Plate	4" x3-1/2"	3,706 lbs	40.7%	21.7%	Unspecified

### **Notes**

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume unbraced length of Top: 00-02-05, Bottom: 00-02-05.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA CONFORMS TO OBC 2012 O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9



DWO NO . TAM 4764617 STRUCTURAL COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1st Floor\...\B7 DR(i1321)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:12

BC CALC® Design Report

City, Province, Postal Code:,

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Dropped Beams\1st Floor\Dropped Beams\B7

Specifier:

Designer: Company:

Misc:

Customer:

Code reports:

**Build 5033** 

Job Name:

Address:

CCMC 12472-R

Connection Diagram

a minimum = 🛊 " b minimum = 3"

Connection design assumes point load is top-loaded. For connection design of side-loaded point loads, please consult a technical representative or professional of Record. Member has no side loads.

Connectors are: 16d Anna Nails
3½ ARDOX SPIRAL

### Disclosure

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DWO NO. FAM 47646-17 STRUCTURAL COMPONENT ONLY



### Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1st Floor\Flush Beams\B8(i1200)

\*

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:13

Build 5033

Job Name: Address:

City, Province, Postal Code:,

BC CALC® Design Report

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Flush Beams\1st Floor\Flush Beams\B8(i1200)

Specifier: Designer:

Company:

Misc:

⊠ 80	07-08-12	B1

Total Horizontal Product Length = 07-08-12

Reaction Summary (De	own / Uplift) ( lbs ) Live	De ad	Snow	Win	d		
B0, 3-1/2"	721/0	379/0					
B1, 3-1/2"	291/0	164/0					
Load Summary		•		Live	Dead	Snow Wind	Trib.
Tag Description	Load Tyne	Ref. Start	End	1.00	0.65	1.00 1.15	

	oad Summary g Description	Load Type	Ref. Start	En d	1.00	0.65	1.00 1.15	1 FID.
Ō	FC2 Floor Material	Unf. Lin. (lb/ft)	L 00-03-	08 07-04-08	3 23	12		n/a
1	Us er Load	Unf. Lin. (lb/ft)	L 00-03-	08 03-09-08	3 240	120		n/a

	Factored	Factored	Demand /	Load	Location
Controls Summary	Dem and	Resistance	Resistance	Case	
Pos. Moment	2,187 ft-lbs	12,704 ft-lbs	17.2%	1	03-00-06
End Shear	1,089 lbs	5,785 lbs	18.8%	1	01-01-00
Total Load Defl.	L/999 (0.054")	n/a	n/a	4	03-07-07
Live Load Defl.	L/999 (0.035")	n/a	n/a	5	03-07-07
Max Defl.	0.054"	n/a	n/a	4	03-07-07
Span / Depth	9.2	n/a	n/a		00-00-00

Poori	na Sunnorts	Dim . (L x W)	De man d	De mand/ Resistance Support	Demand/ Resistance Member	Material
B0 B1	ng Supports Wall/Plate Beam	3-1/2" x 1-3/4" 3-1/2" x 1-3/4"	1,556 lbs 642 lbs	59.4% 12%	20.8% 8.6%	Unspecified Unspecified

### Notes

Design meets Code minimum (L/240) Total load deflection criteria. Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA 086.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

O86.

CONFORMS TO OBC 2012

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

### Disclosure

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DWO NO. TAM 47647-17 STRUCTURAL COMPONENT ONLY



### Boise Cascade Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1st Floor\Flush Beams\B9(i1273)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:13

BC CALC® Design Report

Build 5033 Job Name: Address:

City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Flush Beams\1st Floor\Flush Beams\89(i1273)

Specifier: Designer:

Company:

Misc:

	<u> </u>		$\overline{\mathbb{V}}$
B0		03-05-12	В

Total Horizontal Product Length = 03-05-12

Reaction Summary (I	Down / Uplift) (lbs)				
Bearing	Live	De ad	Snow	Wind	
B0, 2-5/8"	615/0	324/0			
B1, 3-1/2"	571/0	303/0			

Load Summary			Live	Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	En d 1.00	0.65	1.00 1.15	
0 -	Conc. Pt. (lbs)	L 00-11-12	00-11-12 593	297		n/a
1 -	Conc. Pt. (lbs)	L 02-03-12	02-03-12 593	297		n/a

	Factored	Factored	Demand /	Load	Location
Controls Summary	Demand	Resistance	Resistance	Case	
Pos. Moment	1,151 ft-lbs	25,408 ft-lbs	4.5%	1	02-03-12
End Shear	1,266 lbs	11,571 lbs	10.9%	1	01-00-02
Total Load Defl.	L/999 (0.003")	n/a	n/a	4	01-08-07
Live Load Defl.	L/999 (0.002")	n/a	n/a	5	01-08-07
Max Defl.	0.003"	n/a	n/a	4	01-08-07
Span / Depth	3.9	n/a	n/a		00-00-00

Popri	na Sunnorto	Dim. (L x W)	Demand	De mand/ Re sistance Support	Demand/ Resistance Member	Material
B0	<b>ng Supports</b> Post	2-5/8" x 3-1/2"	1,328 lbs	22.3%	11.8%	Unspecified
B1	Post	3-1/2" x 3-1/2"	1,235 lbs	15.5%	8.3%	Unspecified

### Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

CONFORMS TO OBG 2012



DWO NO . TAN 47648.17 STRUCTURAL COMPONENT ONLY



### Boise Cascade Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1st Floor\Flush Beams\B9(i1273)

BC CALC® Design Report



Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:13

Build 5033

Job Name:

Address:

City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

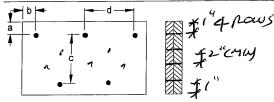
Description: Designs\Flush Beams\1st Floor\Flush Beams\B9(i127;

Specifier:

Designer: Company:

Misc:

### **Connection Diagram**



Calculated Side Load = 434.9 lb/ft

Connection design assumes point load is top-loaded. For connection design of side-loaded point loads, please consult a technical representative or professional of Record.

Connectors are: 16d ARDOX SPIRAL

### Disclosure

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DWG NO .TAM 47648-17 STRUCTURAL COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1st Floor\...\B10(i1279)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:13

BC CALC® Design Report



n/a

**Build 5033** 

Job Name: Address:

City, Province, Postal Code:,

Reaction Summary (Down / Uplift) (lbs)

Customer:

Be aring

B0.5-1/2"

Code reports:

CCMC 12472-R

Live

1,927/0

Conc. Pt. (lbs)

Conc. Pt. (lbs)

File Name: HIGHGROVE 11 EL-2.mmdl

Wind

262

277

Description: Designs\Flush Beams\1st Floor\Flush Beams\B10(i1279)

Specifier: Designer:

Company.

Misc:

1/	2/			3	4
V	, T				
<b>⊠</b> B0		09-0	04-04		B1

Total Horizontal Product	Length = 09	-04-04
--------------------------	-------------	--------

De ad

1.009/0

Snow

07-09-11 525

09-00-00 554

B1, 2-5/8"	2,155 / 0	1,121/0						
Load Summary				Live	Dead	Snow		Trib.
Tag Description	Load Type	Ref. Start	En d	1.00	0.65	1.00	1.15	
0 Smoothed Load	Unf. Lin. (lb/ft)	L 02-07-04	07-07-04	390	195			n/a
1 -	Conc. Pt. (lbs)	L 01-00-08	01-00-08	595	297			n/a
1 - 2	Conc. Pt. (lbs)	1. 02-03-07	02-03-07	447	224			n/a
2 -	Cons Pt (lbs)	1 07-09-11	07-09-11		262			n/a

07-09-11

09-00-00

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	9,243 ft-lbs	25,408 ft-lbs	36.4%	1	05-00-00
End Shear	3,798 lbs	11,571 lbs	32.8%	1	01-03-00
Total Load Defl.	L/585 (0.18")	0.44"	41%	4	04-09-05
Live Load Defl.	L/999 (0.119")	n/a	n/a	5	04-09-05
Max Defl.	0.18"	n/a	n/a	4	04-09-05
Span / Depth	11.1	n/a	n/a		00-00-00

				Demand/ Resistance	Demand/ Resistance	
Bear	ing Supports	Dim . (L x W)	Demand	Support	Member	Material
B0	Wall/Plate	5-1/2" x 3-1/2"	4,152 lbs	50.5%	17.7%	Un spe dified
B1	Post	2-5/8" x 3-1/2"	4,634 lbs	<b>7</b> 7. <b>7</b> %	41.3%	Un spe dified

### Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA 086.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA O86.

Design based on Dry Service Condition.

CONFORMS TO OBC 2012

Importance Factor: Normal Part code: Part 9



DWG NO. TAM 47649-17 STRUCTURAL COMPONENT ONLY



### Double 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1st Floor\...\B10(i1279)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

June 7, 2017 09:38:13

BC CALC® Design Report

**Build 5033** Job Name: Address:

City, Province, Postal Code:,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

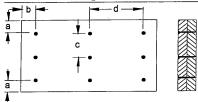
Description: Designs\Flush Beams\1st Floor\Flush Beams\B10(i127

Specifier: Designer:

Company.

Misc:

### Connection Diagram



a minimum = 2"

c = 2-3/4"

4" b minimum = 3"

### Calculated Side Load = 562.6 lb/ft

Connection design assumes point load is top-loaded. For connection design of side-loaded point loads, please consult a technical representative or professional of Record.

Connectors are: 16d Res Nails

312" ARDOX SPIRAL

### Disclosure

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DWG NO. TAM 47649-17 STRUCTURAL COMPONENT ONLY



### Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1st Floor\...\B11 DR(i1372)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

September 18, 2017 10:47:01

BC CALC® Design Report

\*

Build 5033 Job Name:

Address:
City, Province, Postal Code:WATERDOWN,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Dropped Beams\1st Floor\Dropped Beams\B11

Specifier:

Designer: AJ

Company: Misc:

⊠ B0	03-05-14	В1

Total Horizontal Product Length = 03-05-14

Reaction Summary (	(Down / Uplift) (lbs) Live	De ad	Snow	Wind
B0, 5-1/2"		152/0		
B1		168/0		

Load Cummon				Live	Dead	Snow	Wind	Trib.
Load Summary Tag Description	Load Type	Ref. Start	En d	1.00	0.65	1.00	1.15	
0 Us er Load	Unf. Lin. (lb/ft)	L 00-05-08	03-05-14		100			n/a

CONFORMS TO OBG 2012

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	164 ft-lbs	8,258 ft-lbs	2%	0	01-10-11
End Shear	94 lbs	3,761 lbs	2.5%	0	01-03-00
Total Load Defl.	L/999 (0.001")	n/a	n/a	1	01-10-11
Max Defl.	0.001"	n/a	n/a	1	01-10-11
Span / Depth	3.8	n/a	n/a		00-00-00

				De mand/ Resistance			
Bear	ring Supports	Dim.(LxW)	Demand	Support	Member	Material	
B0	Wall/Plate	5-1/2" x 1-3/4"	213 lbs	4.2%	2.8%	Unspecified	
B1	Hanger	2" x 1-3/4"	235 lbs	n/a	8.5%	HUS1.81/10	

### Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Calculations assume member is fully braced.

Hanger Manufacturer: Unassigned

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

### Disclosure

Completeness and accuracy of input must be verified by anyone w ho w ould rely on output as evidence of suitability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered w ood products must be in accordance w ith current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

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DWO NO. TAM 4765017 STRUGTURAL COMPONENT ONLY



### Single 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP 1st Floor\...\B11 DR(i1696)

Dry | 1 span | No cantilevers | 0/12 slope (deg)

September 18, 2017 10:47:37

BC CALC® Design Report



Build 5033 Job Name:

Job Name: Address:

City, Province, Postal Code:WATERDOWN,

Customer:

Code reports:

CCMC 12472-R

File Name: HIGHGROVE 11 EL-2.mmdl

Description: Designs\Dropped Beams\1st Floor\Dropped Beams\B11

Specifier: Designer: AJ

Company:

Misc:

	] ] ] ] ] ] ] ] ] ] ] ]	
<b>X</b> B0	03-05-14	B1

Total Horizontal Product Length = 03-05-14

Reaction Summary (Do	own / Uplift) (lbs) Live	De ad S	Snow	Win	d			
B0, 5-1/2"	47 / 0	195/0	99 / 0					
B1	53 / 0	215/0	110/0					
				Live	Dead	Snow	Wind	Trib.
Load Summary Tag Description	Load Type	Ref. Start	En d	1.00	0.65	1.00	1.15	
0 UserLoad	Unf. Lin. (lb/ft)	L 00-05-08	03-05-14	33	130	69		n/a

Controls Summary	Factore d Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	211 ft-lbs	8,258 ft-lbs	2.6%	0	01-10-11
End Shear	121 lbs	3,761 lbs	3.2%	0	01-03-00
Total Load Defl.	L/999 (0.002")	n/a	n/a	45	01-10-11
Live Load Defl.	L/999 (0.001")	n/a	n/a	61	01-10-11
Max Defl.	0.002"	n/a	n/a	45	01-10-11
Span / Depth	3.8	n/a	n/a		00-00-00

Po oris	ng Supports	Dim . (L x W)	Demand	De mand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	5-1/2" x 1-3/4"	274 lbs	5.4%	3.6%	Unspecified
B1	Hanger	2" x 1-3/4"	461 lbs	n/a	10.9%	HUS1.81/10

### Notes

Design meets Code minimum (L/240) Total load deflection criteria. Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Hanger Manufacturer: Unassigned

Resistance Factor phi has been applied to all presented results per CSA 086.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA COR6.

Unbalanced snow loads determined from building geometry were used in selected product's verification.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

### Disclosure

Completeness and accuracy of input must be verified by anyone w ho w ould rely on output as evidence of suitability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

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DWO NO. YAM 4765217 STRUCTURAL COMPONENT ONLY



### Triple 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

**PASSED** 

### 1st Floor\Flush Beams\B20(i2175)

BC CALC® Design Report

Dry | 1 span | No cant.

February 20, 2018 15:18:19

Build 6215

Job name:

Address: City, Province, Postal Code: WAT...WN

Customer:

Code reports:

CCMC 12472-R

File name:

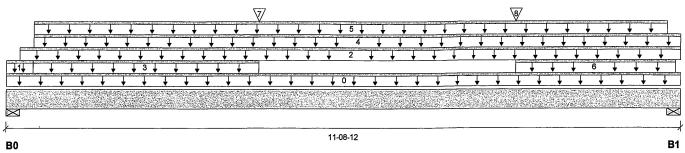
HIGHGROVE 11 EL-2.mmdl

1st Floor\Flush Beams\B20(i2175) Description:

Specifier:

Designer:

Company:



### Total Horizontal Product Length = 11-08-12

Reaction Summary (Down / Uplift) (lbs)

I TOGOLION GAN		/111 c/ \1100/			
Bearing	Live	Dead	Snow	Wind	
B0, 5-1/2"	1,359 / 0	2,484 / 0	2,395 / 0		
B1, 2-3/4"	1,287 / 0	2,645 / 0	2,292 / 0		

Lo	ad Summary					Live	Dead	Snow	Wind	Tributary
	Description	Load Type	Ref.	Start	End	1.00	0.65	1.00	1.15	
0	Self-Weight	Unf. Lin. (lb/ft)	L	00-00-00	11-08-12		14			00-00-00
1	FC2 Floor Material	Unf. Lin. (lb/ft)	L	00-00-00	00-05-07	174				n\a
2	FC2 Floor Material	Unf. Lin. (lb/ft)	L	00-02-12	11-08-12	20	10			n\a
3	ROOF	Unf. Lin. (lb/ft)	L	00-05-08	04-04-08	200	206	562		n\a
4	FC2 Floor Material	Unf. Lin. (lb/ft)	L	00-05-09	11-08-12	6				n\a
5	WALL	Unf. Lin. (lb/ft)	L	00-05-09	11-06-00		77			n\a
6	ROOF	Unf. Lin. (lb/ft)	L	08-10-08	11-07-12	200	206	562		n\a
7	User Load	Conc. Pt. (lbs)	L	04-04-08	04-04-08	450	1,265	464		n\a
8	User Load	Conc. Pt. (lbs)	L	08-10-08	08-10-08	450	1.265	464		n∖a

Controls Summary	Factored Demand	Factored Resistance	Demand/ Resistance	Case	Location
Pos. Moment	18,529 ft-lbs	36,222 ft-lbs	51.2%	13	04-04-08
End Shear	6,179 lbs	17,356 lbs	35.6%	13	01-03-00
Total Load Deflection	L/315 (0.425")	n\a	76.1%	45	05-11-01
Live Load Deflection	L/653 (0.205")	n\a	55.2%	61	05-11-01
Max Defl.	0.425"	n\a	n\a	45	05-11-01
Span / Depth	14.1				

Bearing	g Supports	Dim. (LxW)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	5-1/2" x 5-1/4"	7,377 lbs	47.8%	20.9%	Unspecified
B1	Wall/Plate	2-3/4" x 5-1/4"	7,388 lbs	95.8%	41.9%	Unspecified



STRUCTURAL COMPONENT ONLY





### Triple 1-3/4" x 9-1/2" VERSA-LAM® 2.0 3100 SP

**PASSED** 

February 20, 2018 15:18:19

### 1st Floor\Flush Beams\B20(i2175)

BC CALC® Design Report

**Build 6215** 

Job name:

Address:

City, Province, Postal Code: WAT...WN

Customer:

Code reports:

CCMC 12472-R

Dry | 1 span | No cant.

HIGHGROVE 11 EL-2.mmdl File name:

1st Floor\Flush Beams\B20(i2175) Description:

Specifier:

Designer: ΑJ

**CONFORMS TO OBC 2012** 

Company:

### **Notes**

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA 086.

Unbalanced snow loads determined from building geometry were used in selected product's

verification.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 9

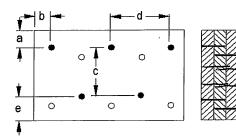
Connection design assumes point load is top-loaded. For connection design of side-loaded point loads,

4 pows

please consult a technical representative or professional of Record. Nailing schedule applies to both sides of the member.

Member has no side loads.

### **Connection Diagram**



a minimum = ? b minimum = 3"

e minimum = 2"

Connection design assumes point load is top-loaded. For connection design of side-loaded point loads, please consult a technical representative or professional of Record. Nailing schedule applies to both sides of the member.

Member has no side loads.

Connectors are: 16d

3-1/2" ARDOX SPIRAL



**Disclosure** Use of the Boise Cascade Software is subject to the terms of the End User License Agreement (EULA). Completeness and accuracy of input must be reviewed and verified by a qualified engineer or other appropriate expert to assure its adequacy, prior to anyone relying on such output as evidence of suitability for a particular application. The output here is based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call (800)232-0788 before installation.

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DWG NO. TAM 9654 STRUCTURAL COMPONENT ONLY





Live Load = 40 psf, Dead Load = 15 psf Simple Spans, L/480 Deflection Limit 5/8" OSB G&N Sheathing







			E	Bare		.1	1/2" Gyp	sum Ceiling	
Depth	Series		On Cent	tre Spacing			On Cent	re Spacing	
		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	NI-20	15'-1"	14'-2"	13'-9"	N/A	15'-7"	14'-8"	14'-2"	N/A
	NI-40x	16'-1"	15' <del>-</del> 2"	14'-8"	N/A	16'-7"	15'-7"	15'-1"	N/A
9 <b>-1/2"</b>	NI-60	16'-3"	15'-4"	14'-10"	N/A	16'-8"	15' <del>-</del> 9"	<b>15'-3</b> "	N/A
	NI-70	17'-1"	16'-1"	15'-6"	N/A	17'-5"	16'-5"	15'-10"	N/A
	NI-80	17'-3"	16'-3"	15'-8"	N/A	17'-8"	16'-7"	16'-0"	N/A
	NI-20	16'-11"	16'-0"	15'-5"	N/A	17'-6"	16'-6"	16'-0"	N/A
	NI-40x	18'-1"	17'-0"	16'-5"	N/A	18'-9"	17'-6"	16'-11"	N/A
11-7/8"	NI-60	18'-4"	17'-3"	16'-7"	N/A	19'-0"	17'-8"	17'-1"	N/A
11 7/0	NI-70	19'-6"	18'-0"	17'-4"	N/A	20'-1"	18'-7"	17'-9"	N/A
	NI-80	19'-9"	<b>18'-</b> 3"	17'-6"	N/A	20'-4"	18'-10"	17'-11"	N/A
	NI-90x	20'-4"	18'-9"	17'-11"	N/A	20'-10"	19'-3"	18'-5"	N/A
	NI-40x	20'-1"	18'-7"	17'-10"	N/A	20'-10"	19'-4"	18' <b>-</b> 6"	N/A
	NI-60	20'-5"	18'-11"	18'-1"	N/A	21'-2"	19'-7"	<b>1</b> 8'-9"	N/A
14"	NI-70	21'-7"	20'-0"	19'-1"	N/A	22'-3"	20'-7"	19'-8"	N/A
	NI-80	21'-11"	20'-3"	19'-4"	N/A	22'-7"	20'-11"	20'-0"	N/A
	NI-90x	22'-7"	20'-11"	19'-11"	N/A	23'-3"	21'-6"	20'-6"	N/A
	NI-60	22'-3"	20'-8"	19'-9"	N/A	23'-1"	21'-5"	20'-6"	N/A
16"	N!-70	23'-6"	21' <b>-</b> 9"	20'-9"	N/A	24'-3"	22'-5"	21'-5"	N/A
	NI-80	23'-11"	22'-1"	21'-1"	N/A	24'-8"	22'-10"	21'-9"	N/A
	NI-90x	24'-8"	22'-9"	21'-9"	N/A	25'-4"	23'-5"	22'-4"	N/A

			Mid-Spa	n Blocking		Mid-S	pan Blocking ar	nd 1/2" Gypsum	Ceiling
Depth	Series		On Cent	re Spacing			On Cent	re Spacing	
		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	NI-20	16'-8"	15'-3"	14'-5"	N/A	16'-8"	15'-3"	14'-5"	N/A
	NI-40x	17'-11"	16'-11"	16'-1"	N/A	18'-5"	17'-1"	16'-1"	N/A
9-1/2"	NI-60	18'-2"	17'-1"	16'-4"	N/A	18'-7"	17'-4"	16'-4"	N/A
	NI-70	19'-2"	17'-10"	17'-2"	N/A	19'-7"	18'-3"	17'-7"	N/A
	NI-80	19'-5"	18'-0"	17'-4"	N/A	19'-10"	18'-5"	17'-8"	N/A
	NI-20	19'-6"	18'-1"	17'-3"	N/A	19'-11"	18'-3"	17'-3"	N/A
	NI-40x	21'-0"	19'-6"	18'-8"	N/A	21'-7"	20'-2"	19'-2"	N/A
11-7/8"	Ni-60	21'-4"	19'-9"	18'-11"	N/A	21'-11"	20'-4"	19'-6"	N/A
11-7/0	NI-70	22'-6"	20'-10"	19'-11"	N/A	23'-0"	21'-5"	20'-5"	N/A
	Ni-80	22'-9"	21'-1"	20'-1"	N/A	23'-3"	21'-7"	20'-8"	N/A
	NI-90x	23'-4"	21'-8"	20'-8"	N/A	23'-10"	22'-2"	21'-2"	N/A
	NI-40x	23'-7"	21'-11"	20'-11"	N/A	24'-3"	22'-7"	21'-7"	N/A
	NI-60	24'-0"	22' <b>-</b> 3"	21'-3"	N/A	24'-8"	22'-11"	21'-11"	N/A
14"	NI-70	25'-3"	23'-4"	22' <b>-</b> 3"	N/A	25'-10"	24'-0"	22'-11"	N/A
	NI-80	25'-7"	23'-8"	22'-7"	N/A	26'-2"	24'-4"	23'-2"	N/A
	NI-90x	26'-4"	24'-4"	23'-3"	N/A	26'-10"	24'-11"	23'-9"	N/A
	NI-60	26'-5"	24'-6"	23'-4"	N/A	27'-2"	25'-3"	24'-2"	N/A
16"	NI-70	27'-9"	25'-8"	24'-6"	N/A	28'-5"	26'-5"	25' <del>-</del> 2"	N/A
10	NI-80	28'-2"	26'-1"	24'-10"	N/A	28'-10"	26'-9"	25'-6"	N/A
	NI-90x	29'-0"	26'-10"	25'-7"	N/A	29'-7"	27'-5"	26'-2"	N/A

<sup>1.</sup> Maximum clear span applicable to simple-span residential floor construction with a design live load of 40 psf and dead load of 15 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration for floor vibration, a live load deflection limit of L/480 and a total load deflection limit of L/240.

<sup>2.</sup> Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum thickness of 5/8 inch for a joist spacing of 19.2 inches or less. The composite floor may include 1/2 inch gypsum ceiling and/or one row of blocking at mid-span with strapping. Strapping shall be minimum 1x4 inch strap applied to underside of joists at blocking line or 1/2 inch gypsum ceiling attached to joists.

<sup>3.</sup> Minimum bearing length shall be 1-3/4 inches for the end bearings.

<sup>4.</sup> Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.

<sup>5.</sup> This span chart is based on uniform loads. For applications with other than uniformly distributed loads, an engineering analysis may be required based on the use of the design properties. Tables are based on Limit States Design per CSA O86-09, NBC 2010, and OBC 2012.

<sup>6.</sup> Joists shall be laterally supported at supports and continuously along the compression edge. Refer to technical documentation for installation guidelines and construction details. Nordic I-joists are listed in CCMC evaluation report 13032-R and APA Product Report PR-L274C.



Live Load = 40 psf, Dead Load = 15 psf Simple Spans, L/480 Deflection Limit 3/4" OSB G&N Sheathing







				are		<b>I</b>	1/2" Gyp	sum Ceiling	
Depth	Series		On Cent	re Spacing			On Cen	tre Spacing	
		12"	16"	19.2"	24"	12"	16"	<b>/</b> 19.2"	24"
	NI-20	15'-10"	15'-0"	14'-5"	13'-5"	16'-4"	15'-5"	14'-6"	13'-5"
	NI-40x	17'-0"	16'-0"	15'-5"	14'-9"	17'-5"	16'-5"	15'-10"	15' <b>-</b> 2"
9-1/2"	NI-60	17'-2"	16'-2"	15'-7"	14'-11"	17'-6"	16'-7"	15'-11"	15'-3"
	NI-70	18'-0"	16'-11"	16'-3"	15'-7"	18'-5"	17'-3"	16'-7"	15'-11"
	NI-80	18'-3"	17'-1"	16'-5"	15'-9"	18'-8"	17'-5"	16'-9"	16'-1"
	NI-20	17'-10"	16'-10"	16'-2"	15'-6"	18'-6"	17'-4"	16'-9"	16'-1"
	NI-40x	19'-4"	17'-11"	17'-3"	16'-6"	19'-11"	18'-6"	17'-9"	17'-0"
11-7/8"	NI-60	19'-7"	18'-2"	17'-5"	16'-9"	20'-2"	18'-9"	17'-11"	17'-2"
11-7/6	NI-70	20'-9"	19'-2"	18'-3"	17'-5"	21'-4"	19'-9"	18'-10"	17'-10"
	NI-80	21'-1"	19'-5"	18'-6"	17'-7"	21'-7"	20'-0"	19'-0"	18'-0"
	NI-90x	21'-8"	20'-0"	19'-1"	18'-0"	22'-2"	20'-6"	19'-6"	18'-6"
	NI-40x	21'-5"	19'-10"	18'-11"	17'-11"	22'-1"	20'-6"	19'-7"	18'-7"
	NI-60	21'-10"	20'-2"	19'-3"	18'-2"	22'-5"	20'-10"	19'-11"	18'-10"
14"	NI-70	23'-0"	21'-3"	20'-3"	19'-2"	23'-8"	21'-11"	20'-10"	19'-9"
	NI-80	23'-5"	21'-7"	20'-7"	19' <b>-</b> 5"	24'-0"	22'-3"	21' <del>-</del> 2"	20'-0"
	NI-90x	24'-1"	22'-3"	21'-2"	20'-0"	24' <del>-</del> 8"	22'-10"	21'-9"	20'-7"
	NI-60	23'-9"	22'-0"	20'-11"	19'-10"	24'-6"	22'-9"	21'-8"	20'-6"
16"	NI-70	25'-1"	23'-2"	22'-0"	20'-10"	25'-9"	23'-10"	22'-9"	21'-6"
10	NI-80	25' <b>-</b> 6"	23'-6"	22'-4"	21'-2"	26'-1"	24'-2"	23'-1"	21'-10"
	NI-90x	26'-4"	24'-3"	23'-1"	21'-10"	26'-11"	24'-11"	23'-8"	22'-5"

			Mid-Spa	n Blocking		Mid-S	Span Blocking a	nd 1/2" Gypsum	Ceiling
Depth	Series		On Cent	re Spacing			On Cent	re Spacing	
		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	NI-20	16'-10"	15'-5"	14'-6"	13'-5"	16'-10"	15'-5"	14'-6"	13'-5"
	NI-40x	18'-8"	17'-2"	16'-3"	15'-2"	18'-10"	17'-2"	16'-3"	15'-2"
9-1/2"	NI-60	18'-11"	17'-6"	16'-6"	15'-5"	19'-2"	17'-6"	16'-6"	15'-5"
	NI-70	20'-0"	18'-7"	17'-9"	16'-7"	20'-5"	18'-11"	17'-10"	16'-7"
	NI-80	20'-3"	18'-10"	17'-11"	16'-10"	20'-8"	19'-3"	18'-2"	16'-10"
	NI-20	20'-1"	18'-5"	17'-5"	16'-2"	20'-1"	18'-5"	17'-5"	16'-2"
	NI-40x	21'-10"	20'-4"	19'-4"	17'-8"	22'-5"	20'-6"	19'-4"	17'-8"
11-7/8"	NI-60	22'-1"	20'-7"	19'-7"	18'-4"	22'-8"	20'-10"	19'-8"	18'-4"
11-7/0	NI-70	23'-4"	21'-8"	20'-8"	19'-7"	23'-10"	22' <b>-</b> 3"	21'-2"	19'-9"
	NI-80	23'-7"	21'-11"	20'-11"	19'-9"	24'-1"	22'-6"	21'-5"	20'-0"
	NI-90x	24'-3"	22'-6"	21'-6"	20'-4"	24'-8"	23'-0"	22'-0"	20'-9"
	NI-40x	24'-5"	22'-9"	21'-8"	19'-5"	25'-1"	23'-2"	21'-9"	19'-5"
	NI-60	24'-10"	23'-1"	22'-0"	20'-10"	25'-6"	23' <b>-</b> 8"	22'-4"	20'-10"
14"	NI-70	26'-1"	24'-3"	23' <del>-</del> 2"	21'-10"	26'-8"	24'-11"	23'-9"	22'-4"
	NI-80	26'-6"	24'-7"	23' <b>-</b> 5"	22'-2"	27'-1"	25'-3"	24'-1"	22'-9"
	NI-90x	27' <b>-</b> 3"	25'-4"	24'-1"	22'-9"	27'-9"	25' <b>-</b> 11"	24'-8"	23'-4"
	NI-60	27'-3"	25'-5"	24'-2"	22'-10"	28'-0"	26'-2"	24'-9"	23'-1"
16"	NI-70	28'-8"	26'-8"	25'-4"	23'-11"	29'-3"	27'-4"	26'-1"	24'-8"
10	NI-80	29'-1"	27'-0"	25'-9"	24'-4"	29'-8"	27'-9"	26'-5"	25'-0"
	NI-90x	29'-11"	27'-10"	26'-6"	25'-0"	30'-6"	28'-5"	27'-2"	25'-8"

<sup>1.</sup> Maximum clear span applicable to simple-span residential floor construction with a design live load of 40 psf and dead load of 15 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration for floor vibration, a live load deflection limit of L/480 and a total load deflection limit of L/240.

<sup>2.</sup> Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum thickness of 3/4 inch for a joist spacing of 24 inches or less. The composite floor may include 1/2 inch gypsum ceiling and/or one row of blocking at mid-span with strapping. Strapping shall be minimum 1x4 inch strap applied to underside of joists at blocking line or 1/2 inch gypsum ceiling attached to joists.

<sup>3.</sup> Minimum bearing length shall be 1-3/4 inches for the end bearings.

<sup>4.</sup> Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.

<sup>5.</sup> This span chart is based on uniform loads. For applications with other than uniformly distributed loads, an engineering analysis may be required based on the use of the design properties. Tables are based on Limit States Design per CSA O86-09, NBC 2010, and OBC 2012.

<sup>6.</sup> Joists shall be laterally supported at supports and continuously along the compression edge. Refer to technical documentation for installation guidelines and construction details. Nordic I-joists are listed in CCMC evaluation report 13032-R and APA Product Report PR-L274C.



Live Load = 40 psf, Dead Load = 30 psf Simple Spans, L/480 Deflection Limit 5/8" OSB G&N Sheathing







				Bare			1/2" Gyp	sum Ceiling	
Depth	Series		On Cen	tre Spacing			On Cent	re Spacing	
		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	Ni-20	15'-1"	14'-1"	13'-3"	N/A	15'-7"	14'-1"	13'-3"	N/A
	NI-40x	16'-1"	15'-2"	14'-8"	N/A	16'-7"	15'-7"	15'-1"	N/A
9 <b>-1/</b> 2"	NI-60	16'-3"	15'-4"	14'-10"	N/A	16'-8"	15'-9"	15'-3"	N/A
	NI-70	17'-1"	16'-1"	15'-6"	N/A	17'-5"	16'-5"	15'-10"	N/A
	NI-80	17'-3"	16'-3"	15'-8"	N/A	17'-8"	16'-7"	16'-0"	N/A
	NI-20	16'-11"	16'-0"	15'-5"	N/A	17'-6"	16'-6"	16'-0"	N/A
	NI-40x	18'-1"	17'-0"	16' <b>-</b> 5"	N/A	18'-9"	17'-6"	16'-11"	N/A
11-7/8"	NI-60	18'-4"	17'-3"	16'-7"	N/A	19'-0"	17'-8"	17'-1"	N/A
11 //0	N!-70	19' <b>-</b> 6"	18'-0"	17'-4"	N/A	20'-1"	18'-7"	17'-9"	N/A
	NI-80	19' <b>-</b> 9"	18'-3"	17'-6"	N/A	20'-4"	18'-10"	17'-11"	N/A
	NI-90x	20'-4"	18'-9"	17'-11"	N/A	20'-10"	19'-3"	18'-5"	N/A
	NI-40x	20'-1"	18'-7"	17'-10"	N/A	20'-10"	19'-4"	18'-6"	N/A
	NI-60	20' <b>-</b> 5"	18'-11"	18'-1"	N/A	21'-2"	19'-7"	18'-9"	N/A
14"	NI-70	21'-7"	20'-0"	19'-1"	N/A	22'-3"	20'-7"	19'-8"	N/A
	NI-80	21'-11"	20'-3"	19'-4"	N/A	22'-7"	20'-11"	20'-0"	N/A
	NI-90x	22'-7"	20'-11"	19'-11"	N/A	23'-3"	21'-6"	20'-6"	N/A
	NI-60	22'-3"	20'-8"	19'-9"	N/A	23'-1"	21'-5"	20'-6"	N/A
16"	NI-70	23'-6"	21'-9"	20'-9"	N/A	24'-3"	22' <del>-</del> 5"	21'-5"	N/A
10	NI-80	23'-11"	22'-1"	21'-1"	N/A	24'-8"	22' <b>-1</b> 0"	21'-9"	N/A
	NI-90x	24'-8"	22'-9"	21'-9"	N/A	25'-4"	23'-5"	22'-4"	N/A

			Mid-Spa	an Blocking		Mid-	Span Blocking a	nd 1/2" Gypsum	Ceiling
Depth	Series		On Cent	re Spacing			On Cent	re Spacing	
		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	NI-20	15'-7"	14'-1"	13'-3"	N/A	15'-7"	14'-1"	13'-3"	N/A
	NI-40x	17'-9"	16'-1"	15'-1"	N/A	17'-9"	16'-1"	15'-1"	N/A
9-1/2"	NI-60	18'-1"	16'-4"	15'-4"	N/A	18'-1"	16'-4"	15'-4"	N/A
	NI-70	19'-2"	17'-10"	16'-9"	N/A	19'-7"	17'-10"	16'-9"	N/A
	NI-80	19'-5"	18'-0"	17'-1"	N/A	19'-10"	18'-3"	17'-1"	N/A
	NI-20	18'-9"	17'-0"	16'-0"	N/A	18'-9"	17'-0"	16'-0"	N/A
	NI-40x	21'-0"	19' <b>-</b> 3"	17'-9"	N/A	21'-3"	19'-3"	17'-9"	N/A
11-7/8"	NI-60	21'-4"	19'-8"	18'-5"	N/A	21'-8"	19'-8"	18'-5"	N/A
//0	NI-70	22'-6"	20'-10"	19'-11"	N/A	23'-0"	21'-4"	20'-0"	N/A
	NI-80	22'-9"	21'-1"	20'-1"	N/A	23'-3"	21'-7"	20'-5"	N/A
	NI-90x	23'-4"	21'-8"	20'-8"	N/A	23'-10"	22' <del>-</del> 2"	21'-2"	N/A
	NI-40x	23'-7"	21'-5"	19'-6"	N/A	24'-1"	21'-5"	19'-6"	N/A
	NI-60	24'-0"	22'-3"	21'-0"	N/A	24'-8"	22'-5"	21'-0"	N/A
14"	N!-70	25'-3"	23'-4"	22'-3"	N/A	25'-10"	24'-0"	22' <b>-</b> 9"	N/A
	NI-80	25 <b>'-7"</b>	23'-8"	22'-7"	N/A	26'-2"	24'-4"	23'-2"	N/A
	NI-90x	26'-4"	24'-4"	23 <b>'-</b> 3"	N/A	26'-10"	24'-11"	23'-9"	N/A
	NI-60	26'-5"	24'-6"	23'-4"	N/A	27'-2"	24'-10"	23'-4"	N/A
16"	NI-70	27'-9"	25'-8"	24'-6"	N/A	28'-5"	26'-5"	25'-2"	N/A
20	NI-80	28' <b>-</b> 2"	26'-1"	24'-10"	N/A	28'-10"	26'-9"	25'-6"	N/A
	NI-90x	29'-0"	26'-10"	25'-7"	N/A	29'-7"	27' <b>-</b> 5"	26'-2"	N/A

<sup>1.</sup> Maximum clear span applicable to simple-span residential floor construction with a design live load of 40 psf and dead load of 30 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration for floor vibration, a live load deflection limit of L/480 and a total load deflection limit of L/240.

<sup>2.</sup> Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum thickness of 5/8 inch for a joist spacing of 19.2 inches or less. The composite floor may include 1/2 inch gypsum ceiling and/or one row of blocking at mid-span with strapping. Strapping shall be minimum 1x4 inch strap applied to underside of joists at blocking line or 1/2 inch gypsum ceiling attached to joists.

<sup>3.</sup> Minimum bearing length shall be 1-3/4 inches for the end bearings.

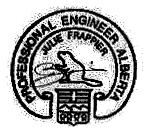
<sup>4.</sup> Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.

<sup>5.</sup> This span chart is based on uniform loads. For applications with other than uniformly distributed loads, an engineering analysis may be required based on the use of the design properties. Tables are based on Limit States Design per CSA O86-09, NBC 2010, and OBC 2012.

<sup>6.</sup> Joists shall be laterally supported at supports and continuously along the compression edge. Refer to technical documentation for installation guidelines and construction details. Nordic I-joists are listed in CCMC evaluation report 13032-R and APA Product Report PR-L274C.



Live Load = 40 psf, Dead Load = 30 psf Simple Spans, L/480 Deflection Limit 3/4" OSB G&N Sheathing







			B	are		I	1/2" Gyp	sum Ceiling	
Depth	Series		On Cent	re Spacing			On Cent	re Spacing	
		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	NI-20	15'-7"	14'-2"	13'-4"	12'-4"	15'-7"	14'-2"	13'-4"	12'-4"
	NI-40x	17'-0"	16'-0"	15'-1"	13'-11"	17'-5"	16'-1"	15'-1"	13'-11"
9-1/2"	NI-60	17'-2"	16'-2"	15'-5"	14'-3"	17'-6"	16'-5"	15'-5"	14'-3"
	NI-70	18'-0"	16'-11"	16'-3"	15'-6"	18'-5"	17'-3"	16'-7"	15'-6"
	NI-80	18'-3"	17'-1"	16'-5"	15'-9"	18'-8"	17'-5"	16'-9"	15'-10"
	NJ-20	17'-10"	16'-10"	16'-0"	14'-10"	18'-6"	17'-1"	16'-0"	14'-10"
	NI-40x	19'-4"	17'-11"	17' <b>-</b> 3"	15'-10"	19'-11"	18'-6"	<b>17'-9</b> "	15'-10"
11-7/8"	NI-60	19'-7"	18'-2"	17'-5"	16'-9"	20'-2"	18'-9"	17'-11"	17'-1"
11-7/6	NI-70	20'-9"	19' <b>-</b> 2"	18'-3"	17'-5"	21'-4"	19' <b>-</b> 9"	18'-10"	17'-10"
	NI-80	21'-1"	19'-5"	18'-6"	17'-7"	21'-7"	20'-0"	19'-0"	18'-0"
	NI-90x	21'-8"	20'-0"	19'-1"	18'-0"	22'-2"	20'-6"	19'-6"	18'-6"
	NI-40x	21'-5"	19'-10"	18'-11"	17'-5"	22'-1"	20'-6"	19'-6"	17'-5"
	NI-60	21'-10"	20'-2"	19'-3"	18'-2"	22'-5"	20'-10"	19'-11"	18'-10"
14"	NI-70	23'-0"	21'-3"	20'-3"	19'-2"	23'-8"	21'-11"	20'-10"	19'-9"
	NI-80	23'-5"	21 <b>'-</b> 7"	20'-7"	19'-5"	24'-0"	22' <del>-</del> 3"	21'-2"	20'-0"
	NI-90x	24'-1"	22' <b>-</b> 3"	21'-2"	20'-0"	24'-8"	22'-10"	21'-9"	20'-7"
	NI-60	23'-9"	22'-0"	20'-11"	19'-10"	24'-6"	22'-9"	21'-8"	20'-6"
16"	NI-70	25'-1"	23'-2"	22'-0"	20'-10"	25'-9"	23'-10"	22' <del>-</del> 9"	21'-6"
10	NI-80	25 <b>'-</b> 6"	23'-6"	22'-4"	21'-2"	26'-1"	24'-2"	23'-1"	21'-10"
	NI-90x	26'-4"	24'-3"	23'-1"	21'-10"	26'-11"	24'-11"	23' <b>-</b> 8"	22'-5"

			Mid-Spa	n Blocking		Mid-S	pan Blocking ar	nd 1/2" Gypsum	Ceiling
Depth	Series		On Cent	re Spacing			On Cent	re Spacing	
		12"	16"	19.2"	24"	12"	16"	19.2"	24"
	NI-20	15'-7"	14'-2"	13'-4"	12'-4"	15'-7"	14'-2"	13'-4"	12'-4"
	NI-40x	17'-9"	16'-1"	15'-1"	13'-11"	17'-9"	16'-1"	15'-1"	13'-11'
9-1/2"	NI-60	18'-1"	16'-5"	15'-5"	14'-3"	18'-1"	16'-5"	15'-5"	14'-3"
	NI-70	19'-10"	17'-11"	16'-9"	15'-6"	19'-10"	17'-11"	16'-9"	15'-6"
	NI-80	20'-2"	18'-3"	17'-1"	15'-10"	20'-2"	18'-3"	17'-1"	15'-10'
.,	NI-20	18'-10"	17'-1"	16'-0"	14'-10"	18'-10"	17'-1"	16'-0"	14'-10'
	Ni-40x	21'-3"	19'-3"	17'-9"	15'-10"	21'-3"	19'-3"	17'-9"	15'-10'
11-7/8"	NI-60	21'-9"	19'-8"	18'-5"	17'-1"	21'-9"	19'-8"	18'-5"	17'-1"
11-//0	NI-70	23'-4"	21' <del>-</del> 5"	20'-1"	18'-6"	23'-8"	21'-5"	20'-1"	18'-6"
	NI-80	23'-7"	21'-10"	20'-5"	18'-11"	24'-1"	21'-10"	20'-5"	18'-11
	NI-90x	24'-3"	22'-6"	21'-3"	19'-7"	24'-8"	22'-7"	21'-3"	19'-7"
	NI-40x	24'-2"	21'-5"	19'-6"	17'-5"	24'-2"	21'-5"	19'-6"	17' <b>-</b> 5"
	NI-60	24'-9"	22'-5"	21'-0"	19'-6"	24'-9"	22' <b>-</b> 5"	21'-0"	19'-6"
14"	NI-70	26'-1"	24'-3"	22 <b>'-</b> 9"	21'-0"	26'-8"	24'-3"	22' <b>-</b> 9"	21'-0"
	NI-80	26'-6"	24'-7"	23'-3"	21'-6"	27'-1"	24'-10"	23' <b>-</b> 3"	21'-6"
	NI-90x	27' <b>-</b> 3"	25'-4"	24'-1"	22'-4"	27' <b>-</b> 9"	25'-10"	24'-3"	22'-4"
	NI-60	27'-3"	24'-11"	23'-5"	21'-7"	27'-6"	24'-11"	23'-5"	21'-7"
16"	NI-70	28'-8"	26'-8"	25'-3"	23'-4"	29'-3"	26'-11"	25' <b>-</b> 3"	23'-4"
10	NI-80	29'-1"	27'-0"	25'-9"	23'-10"	29'-8"	27'-6"	25'-10"	23'-10"
	NI-90x	29'-11"	27'-10"	26'-6"	24'-10"	30'-6"	28' <b>-</b> 5"	26'-11"	24'-10'

<sup>1.</sup> Maximum clear span applicable to simple-span residential floor construction with a design live load of 40 psf and dead load of 30 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration for floor vibration, a live load deflection limit of L/480 and a total load deflection limit of L/240.

<sup>2.</sup> Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum thickness of 3/4 inch for a joist spacing of 24 inches or less. The composite floor may include 1/2 inch gypsum ceiling and/or one row of blocking at mid-span with strapping. Strapping shall be minimum 1x4 inch strap applied to underside of joists at blocking line or 1/2 inch gypsum ceiling attached to joists.

<sup>3.</sup> Minimum bearing length shall be 1-3/4 inches for the end bearings.

<sup>4.</sup> Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.

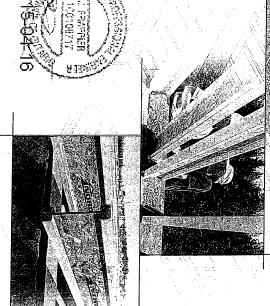
<sup>5.</sup> This span chart is based on uniform loads. For applications with other than uniformly distributed loads, an engineering analysis may be required based on the use of the design properties. Tables are based on Limit States Design per CSA O86-09, NBC 2010, and OBC 2012.

<sup>6.</sup> Joists shall be laterally supported at supports and continuously along the compression edge. Refer to technical documentation for installation guidelines and construction details. Nordic I-joists are listed in CCMC evaluation report 13032-R and APA Product Report PR-L274C.



## NSTALLATION GUIDE ENGINEERED WOOD

FOR RESIDENTIAL FLOORS



Distributed by:



# SAFETY AND CONSTRUCTION PRECAUTIONS



braced, or serious inju-Do not walk on I-joists until fully fastened and ries can result.



over-stress I-joist with concentrated loads from Once sheathed, do not materials over unsheathed I-joists. Never stack building building materials.



N-C301 / November 2014

braced and sheathed I-joists are not stable until completely installed, and will not carry any load until fully

# Avoid Accidents by Following these Important Guidelines:

- 1. Brace and nail each 1-joist as it is installed, using hangers, blocking panels, rim blocking will be required at the interior support. over interior supports and a load-bearing wall is planned at that location, board, and/or cross-bridging at joist ends. When I-joists are applied continuous
- 2. When the building is completed, the floor sheathing will provide lateral to prevent I-joist rollover or buckling. remporary bracing, often called struts, or temporary sheathing must be applied support for the top flanges of the 1-joists. Until this sheathing is applied,
- Temporary bracing or struts must be 1x4 inch minimum, at least 8 feet long the bracing to a lateral restraint at the end of each bay. Lap ends of adjoining minimum of two 2-1/2" nails fastened to the top surface of each I-joist. Nail bracing over at least two I-joists. and spaced no more than 8 feet on centre, and must be secured with a
- Or, sheathing (temporary or permanent) can be nailed to the top flange of the first 4 feet of I-joists at the end of the bay.
- 3. For cantilevered I-joists, brace top and bottom flanges, and brace ends with closure panels, rim board, or cross-bridging.
- 4. Install and fully nail permanent sheathing to each 1-joist before placing loads on the floor system. Then, stack building materials over beams or walls only
- Never install a damaged I-joist.

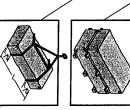
can result in serious accidents. Follow these installation guidelines carefully Improper storage or installation, failure to follow applicable building codes, failure to follow span ratings for Nordic Hoists, failure to follow allowable hole sizes and locations, or failure to use web stiffeners when required

# STORAGE AND HANDLING GUIDELINES

- 1. Bundle wrap can be slippery when wet. Avoid walking on wrapped

Store, stack, and handle I-joists vertically and level only.

- 3. Always stack and handle I-joists in the upright position only.
- Protect I-joists from weather, and use spacers to separate bundles. 4. Do not store I-joists in direct contact with the ground and/or flatwise
- Bundled units should be kept intact until time of installation.
- 7. When handling Lioists with a crane on the job site, take a few simple precautions to prevent damage to the Lipists and injury
- Pick I-joists in bundles as shipped by the supplier
- Orient the bundles so that the webs of the I-joists are vertical.
- ■Pick the bundles at the 5th points, using a spreader bar if necessary.
- Do not handle I-joists in a horizontal orientation
- 9. NEVER USE OR TRY TO REPAIR A DAMAGED I-JOIST.





## MAXIMUM FLOOR SPANS

- or more of the adjacent span. For multiple-span applications, the end spans shall be 40% for floor vibration and a live load deflection limit of L/480 live load of 40 psf and dead load of 15 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration nultiple-span residential floor construction with a design
- Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum Standard. No concrete topping or bridging element was assumed. Increased spans may be achieved with the used thickness of 5/8 inch for a joist spacing of 19.2 inches or less, or 3/4 inch for joist spacing of 24 inches. Adhesive shall meet the requirements given in CGBS-71.26 of gypsum and/or a row of blocking at mid-span.
- Minimum bearing length shall be 1-3/4 inches for the end bearings, and 3-1/2 inches for the intermediate bearings.

Bearing stiffeners are not required when I-joists are used

- 5. This span chart is based on uniform loads. For applications
- with other than uniform loads, an engineering analysis may be required based on the use of the design properties.
- O86-09 Standard, and NBC 2010.

## SIMPLE AND MULTIPLE SPANS MAXIMUM FLOOR SPANS FOR NORDIC I-JOISTS

**I-JOIST HANGERS** 

Hangers shown illustrate the three

most commonly used metal hangers

Hangers should be selected based

on the joist depth, flange width and load capacity based on the

maximum spans.

4. Web stiffeners are required when the

sides of the hangers do not laterally

brace the top flange of the I-joist.

2. All nailing must meet the hanger

manutacturer's recommendations.

to support 1-joists.

				Jeist Depih
				Jois! Series
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21-10 23-0 23-0 23-9	-85446 1.003			N F

CCMC EVALUATION REPORT 13032-R

Top Mour

Face Mount

- Maximum clear spans applicable to simple-span or
- required for hangers. spans and spacings given in this table, except as
- 6. Tables are based on Limit States Design per CAN/CSA
- 7. SI units conversion: 1 inch = 25.4 mm 1 foot =  $0.305 \, \text{m}$

## WEB STIFFENERS

### RECOMMENDATIONS:

- Construction Guide (C101).The gap between the stiffener and the flange is at the top. reactions greater than shown in the engineered applications with factored A bearing stiffener is required in all -joist properties table found of the I-joist
- sides of the hanger do not extend up to, and the I-joist is supported in a hanger and the stiffener and flange is at the top. support, the top flange. The gap between the A bearing stiffener is required when
- by the code. The gap between the stiffener than 2,370 lbs is applied to the top flange and the flange is at the bottom. adjusted tor other load durations as permitted standard term load duration, and may be tip and the support. These values are for cantilever, anywhere between the cantilever between supports, or in the case of a where a factored concentrated load greater A load stiffener is required at locations

SI units conversion: 1 inch = 25.4 mm

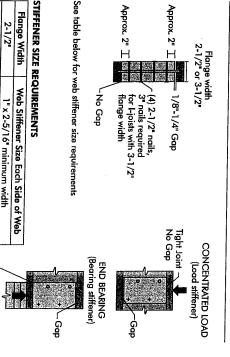
3-1/2"

1-1/2" x 2-5/16" minimum width

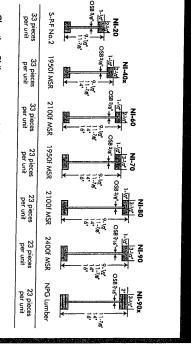
Tight Join

### FIGURE 2

## WEB STIFFENER INSTALLATION DETAILS



## NORDIC I-JOIST SERIES



products to adhere to strict quality control procedures throughout the manufacturing process. Every phase of the operation, from forest to the Chantiers Chibougamau Ltd. harvests its own trees, which enables Nardic finished product, reflects our commitment to quality.

longer span carrying capacity. lumber in their flanges, ensuring consistent quality, supe(for strength ப்றவ Nordic Engineered Wood I-joists use only finger-jointed back spruce

2015-04-16

## INSTALLING NORDIC I-JOISTS

- 1. Before laying out floor system components, verify that I-joist flange widths match hanger widths. If not, containing
- 2. Except for cutting to length, I-joist flanges should never be cut, drilled, or notched.
- 3. Install I-joists so that top and bottom flanges are within 1/2 inch of true vertical alignment

- 4. I-joists must be anchored securely to supports before floor sheathing is attached, and supports for multiple அளில்க்கு nust
- 5. Minimum bearing lengths: 1-3/4 inches for end bearings and 3-1/2 inches for intermediate bearings 1045-04-16
- 6. When using hangers, seat I-joists firmly in hanger bottoms to minimize settlement.
- 7. Leave a 1/16-inch gap between the I-joist end and a header.
- 8. Concentrated loads greater than those that can normally be expected in residential construction should only be applied to the top surface of the top flange. Normal concentrated loads include track lighting fixtures, audio equipment and security cameras. Never suspend unusual or heavy loads from the I-joist's bottom flange. Whenever possible, suspend all concentrated loads from the top of the I-joist. Or, attach the load to blocking that has been securely fastened to the
- 9. Never install I-joists where they will be permanently exposed to weather, or where they will remain in direct contact with
- 10. Restrain ends of floor joists to prevent rollover. Use rim board, rim joists or Ljoist blocking panels
- 11. For I-joists installed over and beneath bearing walls, use full depth blocking panels, rim board, or squash blocks (cripple members) to transfer gravity loads through the floor system to the wall or foundation below.
- 12. Due to shrinkage, common framing lumber set on edge **may never** be used as blocking or rim boards. I joist blocking 1-joist-compatible depth selected. panels or other engineered wood products – such as rim board – must be cut to fit between the I-joists, and an
- 13. Provide permanent lateral support of the bottom flange of all I-joists at interior supports of multiple-span joists. Similarly, support the bottom flange of all cantilevered I-joists at the end support next to the cantilever extension. In the completed structure, the gypsum wallboard ceiling provides this lateral support. Until the final finished ceiling is applied, temporary bracing or struts must be used
- 14. If square-edge panels are used, edges must be supported between Lipists with 2x4 blocking. Glue panels to blocking to minimize squeaks. Blocking is not required under structural finish flooring, such as wood strip flooring, or it a separate underlayment layer is installed
- 15. Nail spacing: Space nails installed to the flange's top face in accordance with the applicable building code requirements or approved building plans.

### top plate per detail 1b Attach I-joist to with same nailing plate (when used for lateral shear as required for transter, nail to 2-1/2" nails at bearing plate 6" o.c. to top

**a** 

panel NI blocking

€

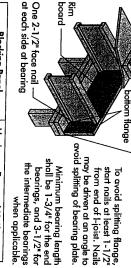
wire or spiral nail at top and One 2-1/2"

plate using 2-1/2" wire or spiral toe-nails at 6" o.c. Attach rim board to top

ottom flange

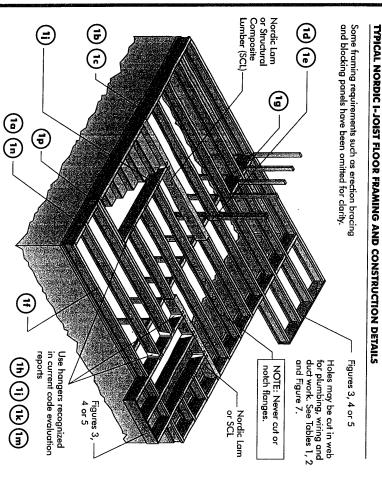
NI Joists	Blocking Panel or Rim Joist
3,300	Maximum Factored Uniform Vertical Load* (plf)

It shall not be used in the design of a bending member, inches or less and is based on standard term load duration such as joist, header, or rafter. For concentrated vertical The uniform vertical load is limited to a joist depth of 16

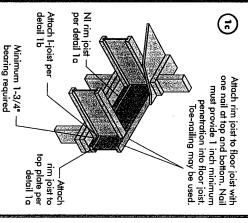


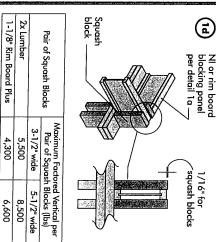
_	
1-1/8" Rim Board Plus	Blocking Panel or Rim Joist
8,090	Maximum Factored Uniform Vertical Load* (pH)

\*The uniform vertical load is limited to a rim board depth of 16 inches or less and is based on standard term load duration. It shall not be used in the design of a bending member, such as joist, header, or after. For concentrated vertical load transfer, see detail 1d



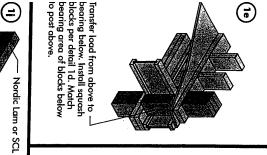
All nails shown in the above details are assumed to be common wire nails unless otherwise noted. 3" (0.122" dia.) common spiral nails may be substituted for 2-1/2" (0.128" dia.) common wire nails. Framing lumber assumed to be Spruce-Pine-Fir No. 2 or better. Individual components not shown to scale for clarity.

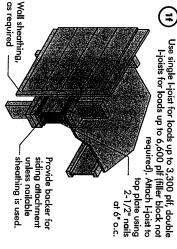




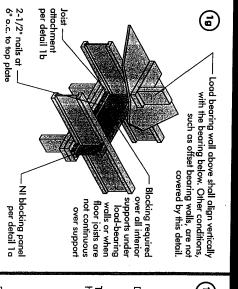
Pair of Squash Blocks	Maximum Factored Vertical per Pair of Squash Blocks (lbs)	red Vertical per h Blocks (lbs)
- denote a comp	3-1/2" wide	5-1/2" wide
2x Lumber	5,500	8,500
1-1/8" Rim Board Plus	4 300	000 7

Provide lateral bracing per detail 1a, 1b, or 1c





required when rim board is used. Bracing per code shall be



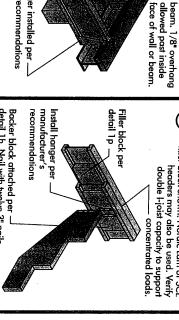
Rim board may be used in lieu of Ljoists. Backer is not carried to the foundation.

(F

**3** 

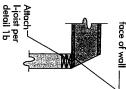
filler block shown. Nordic Lam or SCL Multiple I-joist header with full depth

allowed past inside inside face of wall or 2x plate flush with



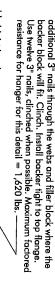
clinch when possible. Maximum support capacity = 1,620 lbs detail 1h. Nail with twelve 3" nails,

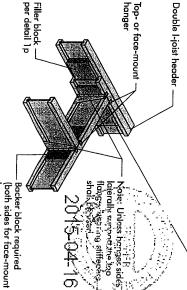




support, not shown at bearing for lateral Note: Blocking required







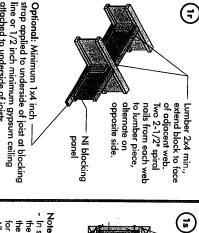
For hanger capacity see hanger manufacturer's recommendations. Verify double I-joist capacity to support concentrated loads

nangers)

BACKER BLOCKS (Blocks must be long enough to permit required nailing without splitting)

lange Width	Material Thickness Required*	Minimum Depth**
2-1/2"	1"	5-1/2"
3-1/2"	1-1/2"	7-1/4"

- Minimum grade for backer block material shall be S-P-F No. 2 or to CAN/CSA-O325 or CAN/CSA-O437 Standard better for solid sawn lumber and wood structural panels conforming
- For face-mount hangers use net joist depth minus 3-1/4" for minus 4-1/4" joists with 1-1/2" thick flanges. For 2" thick flanges use net depth

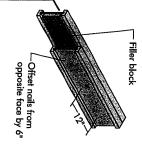


strap applied to underside of joist at blocking Optional: Minimum 1x4 inch line or 1/2 inch minimum gypsum ceiling affached to underside of joists

### (<u>s</u> board S S -One 2-1/2" nails at top and bottom flange One 2-1/2" nails one side only 2-1/2" nails at 6" o.c. lumber piece īwo 2-1/2" nails from each web to I-joist blocking panel ·2x4 min. (1/8" gap minimum)

- In some local codes, blocking is prescriptively required in the starter joist. Where required, see local code requirements the first joist space (or first and second joist space) next to for spacing of the blocking

All nails are common spiral in this detail



—1/8" to 1/4" gap between top flange and filler block ω

€

Note: Unless hanger sides laterally

stiffeners shall be used support the top flange, bearing

support the top flange, bearing stiffeners shall be used. Note: Unless hanger sides laterally manufacturer's recommendations lop-mount hanger installed per ...

recommendations

beams, see the manutacturer's For nailing schedules for multiple recommendations installed per manufacturer's

Top- or face-mount hanger -

1. Support back of I-joist web during nailing to prevent damage to web/flange connection.

DOUBLE I-JOIST CONSTRUCTION

Lumber 2x4 min.,

FILLER BLOCK REQUIREMENTS FOR

2. Leave a 1/8 to 1/4-inch gap between top of filler block and bottom of top I-joist

Flange Size

Joist

Filler block is required between joists for full length of span.

2-1/2"× 1-1/2"

ď. 4 11-7/8" Depth

2-1/8" x 10" 2-1/8" x 12" 2-1/8 x 8" 2-1/8" x 6" Filler Block Size

ှ ယူ \* စု ၀ူ

9-1/2

Nail joists together with two rows of 3 can be clinched, only two nails per foot nails at 12 inches o.c. (clinched when are required. possible) on each side of the double 1-joist. Total of four nails per foot required. If nails

3-1/2"× 1-1/2"×

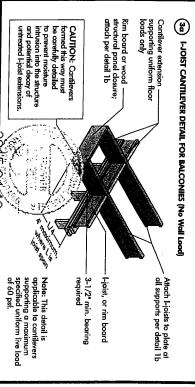
ç

The maximum factored load that may be using this detail is 860 lbf/ft. Verify double applied to one side of the double joist

3-1/2" x 2"

3" × 7" 3º × 10º 3º × 12º ယူ × ဇူ

# CANTILEVER DETAILS FOR BALCONIES (NO WALL LOAD)



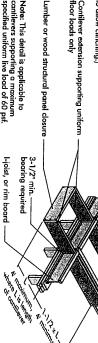


2x8 min. Nail to backer block and joist with 2 rows of 3" nails at 6" o.c. and clinch. (Cantilever nails may be used to attach backer block if length of nail is sufficient Full depth backer block with  $1/8^{\circ}$  gap between block and top flange of L-joist. See detail 1h. Nail with 2 rows of  $3^{\circ}$  nails at  $6^{\circ}$  o.c. and clinch. to allow clinching.)

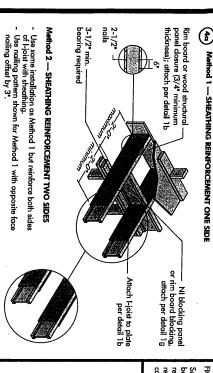
> plate at all supports per detail 1b Attach I-joists to

ttoor loads only Contilever extension supporting uniform

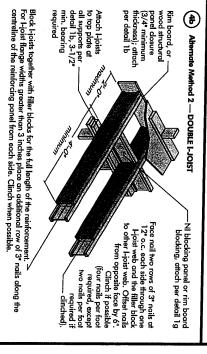
cantilevers supporting a maximum specified uniform live load of 60 psf. Note: This detail is applicable to



# CANTILEVER DETAILS FOR VERTICAL BUILDING OFFSET (CONCENTRATED WALL LOAD)



Note: Canadian softwood plywood sheathing or equivalent (minimum thickness 3/4") required on sides of joist. Depth shall match the full height of the joist. Nail with 2-1/2" rails at 6" o.c., top and bottom flange. Install with tace grain horizontal. Attach I-joist to plate at all supports per detail 1b. Verify reinforced I-joist capacity.



reinforcement FIGURE 4 (continued) requirements at cantilever. below for NI See table Roof truss span -maximum cantilever <u>ي</u> 12 Girder Roof truss Jack trusses truss Roof trusses Koot truss. span 2-0 – 13'–0" maxi

						3	
be used.	26 ft. shall be permitted to	requirements for a span of	the I-joist reinforcement	the cantilevered floor joists,	trusses running parallel to	For hip roofs with the jack	

# CANTILEVER REINFORCEMENT METHODS ALLOWED

5	,	1157.84	9 72	JOIST DEPTH (in.)
26 228 32 34 34 40	26 28 30 32 34 38	26 30 32 34 34 38	6 4 2 0 8 6	ROOF TRUSS SPAN (ff)
ZZZZZZZZZ	100,000		ZZZZZZ	IL = 30 IOIS
ZZZZZZZZZ ZZZZZZZZ		ZZZZZZ		) psf, DL = 1 SPACING (i
zzzz	5 - 5 Z Z Z	3884-145	×××××	5 psf n.) 24
ZZZZZZZZZ		ZZZZZZZ	-22222 -2222	ROOF LÕADIN LL = 40 ps JOIST SI
	zzzz,			ING (UNFAC psf, DL = 15 SPACING (ir 5 19.2
νν <b>-</b> Σ	<- = ' α α α	(××××××××	×××××	TORED) psf .)
ZZZZZZZZ	. <del> </del>	ZZZZZZ	ZZ	μ = 5 1013 1016
-ZZZZZZZ		יביבים	<******	0 psf, DL = 1 77 SPACING (
××	×==ממממ×	*****		5 p <u>s</u>

- 1. N = No reinforcement required.
  1 = NI reinforced with 3/4 wood shudurol panel on one side only.
  2 = NI reinforced with 3/4 wood shudurol panel on both sides, or double I-joist.
  X = If ya desper joist or doser specing.
  Awadmum design load shall be: 15 pef roof deed load, 55 pef floor total load, and 80 pff wall load. Wall load is based on 3-0-0 maximum width window or door openings.
- For larger openings, or multiple 3'-0" width opinings spaced less than 6'-0' c.c., additional joist beneath the opening's cripple students of the property of the property of the students of the property of the students of the space to joist 12' to 24' c.c. that meet the floor span requirements for a design live load of 40 per and level load of 15 per and a live load deflection limit of L480, Uses 12' o.c. requirements for lesser spacing.
  - 4. For conventional roof construction using a ridge beam, the Roof Truss Span column above is equivalent to the distance between the supporting wall and the ridge beam. When the roof is formed using a ridge board, when the roof is formed using a ridge board, the Roof Truss Span is equivalent to the distance between the supporting walls as if a
- truss is used.

  5. Cantilevered joists supporting girder trusses or roof beams may require additional

# RULES FOR CUTTING HOLES AND DUCT CHASE OPENINGS:

- The distance between the inside edge of the support and the centreline of any lable 1 or 2, respectively. hole or duct chase opening shall be in compliance with the requirements of
- I-joist top and bottom flanges must NEVER be cut, notched, or otherwise modified
- Whenever possible, field-cut holes should be centred on the middle of the web.
- 4. The maximum size hole or the maximum depth of a duct chase opening that can be cut into an I-joist web shall equal the clear distance between the flanges of the I-joist minus 1/4 inch. A minimum of 1/8 inch should always be maintained between the top or bottom of the hole or opening and the adjacent I-joist flange.
- Ċ The sides of square holes or longest sides of rectangular holes should not exceed 3/4 of the diameter of the maximum round hole permitted at that location.
- ٥ Where more than one hole is necessary, the distance between adjacent hole opening shall be sized and located in compliance with the requirements of size of the largest square hole (or twice the length of the longest side of the longest rectangular hole or duct chase opening) and each hole and duct chase edges shall exceed twice the diameter of the largest round hole or twice the ables 1 and 2, respectively
- A knockout is **not** considered a hole, may be utilized anywhere it occurs, and may be ignored for purposes of calculating minimum distances between holes and/or duct chase openings.
- œ Holes measuring 1-1/2 inches or smaller shall be permitted anywhere in a cantilevered section of a joist. Holes of greater size may be permitted subject to
- A 1-1/2 inch hole or smaller can be placed anywhere in the web provided that it meets the requirements of rule number 6 above.
- All holes and duct chase openings shall be cut in a workman-like manner in accordance with the restrictions listed above and as illustrated in Figure 7.
- 11. Limit three maximum size holes per span, of which one may be a duct chase
- 12. A group of round holes at approximately the same location shall be permitted if they meet the requirements for a single round hole circumscribed around them.

## Simple or Multiple Span for Dead Loads up to 15 psf and Live Loads up to 40 psf LOCATION OF CIRCULAR HOLES IN JOIST WEBS

<ul> <li>Above table</li> </ul>					Doja
s may be used	-1-1-1- <i>1</i> -	eluleleje,			Joist Series
d for I-joist					
spacing of				lada, jok	5
24 inches	La de la compa			in the unit	3
les on centre or les					" C
or less		LEADING.	eliota. Partogr		##. # . H
	1500100000			10,000	
	THE RESERVE OF THE PERSON NAMED IN COLUMN				
					•
ı	1:00000000			120010	
			BLD LT.		3 - 3
					•
200					

- 2. Hole location distance is measured from inside foce of supports to centre of hole.

  3. Distances in this chart are hereaf an instrument to the supports to centre of hole. Distances in this chart are based on uniformly loaded joists.

### OPTIONAL:

The above table is based on the Hoists used at their maximum span. If the Hoists are placed at less than their full maximum span (see Maximum Fico) Spairs, the minimum distance from the centreline of the hole to the face of any support (D) as given above may be reduced as follows:

 $\frac{\mathsf{D}_{\mathsf{reduced}} = \frac{\mathsf{L}_{\mathsf{actual}}}{\mathsf{SAF}} \times \mathsf{D}$ 

Where: Dreduced =

Lactual Distance from the inside face of any support to centre of hole, reduced for less-than-maximum span applicanes as the distance shall not be less than 6 inches from the face of the support to edge of the hole.

The actual measured span distance between the inside faces of supports (ft)

¥ Span Adjustment Factor given in this table.

The minimum distance from the inside face of any support to centre of hole from this table If <u>Lactual</u> is greater than 1, use 1 in the above calculation for <u>Lactual</u>

2015-04-16

TABLE 2

for the contractor's convenience to instal Knockouts are prescored holes provided DUCT CHASE OPENING SIZES AND LOCATIONS - Simple Span Only

Joisi	Jois	Minimur		e from in	iside face	of clays	upper le			
Dapih	Series	<b>6</b>	ā	Ñ	7 K	use leng	# (fn.)	20	3	e K
	, i	(S.E.)	in k 6012,				12	9.6	7	
	. i . i		in in Unit	512 510	60 47			уш 3.02	i G	- 40 - 40 - 40
			6-24						e ka e ka	. bi
					in 10 	Z.		0 sp 6 dy		
							6 e	6		
				loa 21	88 5	9 4 412	0 S		10.7	
				96	9.6				20	3
				2 ) 2 ) 2 )	70 70	i L		i. Ka		2 4 4
			9-8		j.		15		'n.	12.1 12.1 1
				66 66	i.		12-6		J.	
		100		96	) 2	NN 6	20 23 24		16	
							一年 一日 一日	6		

- Above table may be used for Lioist spacing of 24 inches on centre or less.
   Duct chase opening location distance is measured from inside face of supports to centre of opening.
   The above table is based on simple-span joists only. For other applications, contact your local distributor.
   Distances are based on uniformly located floor joists that meet the span requirements for a design live load of 40 psf and dead load of 15 psf, and a live load deflection limit of U480. For other applications, contact your local distributor.

and may be ignored for purposes of calculating minimum distances A knockout is NOT considered a hole, may be utilized wherever it occurs

Knockouts

See rule 12

all duct chase openings and holes between top and bottom flange ---Maintain minimum 1/8" space Θ

electrical or small plumbing lines. They are 1-1/2 inches in diameter, and are spaced 15 inches on centre along the length of the I-joist. Where possible, it is preferable to use knockouts instead of field-cut holes notch the flange, over-cut the web. sharp saw. should be cut with a Holes in webs Never drill, cut or

٩

bearing -

distance trom for minimum

of larger hole 2x diameter

diameter, length or hole 2x duct chase

Duct chase opening

whichever is

from bearing) minimum distance (see Table 2 for FIELD-CUT HOLE LOCATOR

FIGURE 7

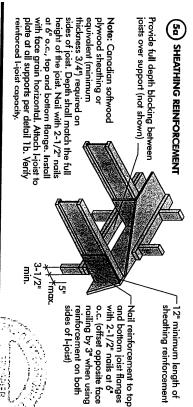
the corners, as this can cause unnecessary stress concentrations. Slightly rounding and then making the cuts between diameter hole in each of the four corners the holes is another good method to the rectangular hole by drilling a 1-inch the corners is recommended. Starting For rectangular holes, avoid over-cutting

ninimize damage to the I-joist

# BRICK CANTILEVER DETAILS FOR VERTICAL BUILDING OFFSET (CONCENTRATED WALL LOAD)

FIGURE 5 (continued)

See table



o.c. (offset opposite face nailing by 3" when using and bottom joist flanges with 2-1/2" nails at 6"

SET-BACK DETAIL

Rim board or wood structural panel closure (3/4" minimum thickness),

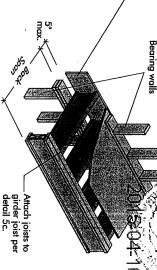
attach per detail 1b.

**(5**b)

Provide full depth blocking

Attach I-joist to plate at all (not shown for clarity)

supports per detail 1b. 3-1/2" minimum I-joist bearing required.



## (5c) SET-BACK CONNECTION

through joist web and web of girder using 2-1/2" nails. Alternate for opposite side, (2x6 S-P-F No. 2 or better) nailed Vertical solid sawn blocks –

> bottom flanges. nails, toe-nail at top and Nail joist end using 3"

Hanger may be



1. N = No reinforcement required.
1 = NI reinforced with 3/4" wood structural panel on one side only.
2 = NI reinforced with 3/4" wood structural panel on both sides, or double 1-joist.
X = Try a deeper joist or closer spacing.
2. Maximum design load shall be: 15 psf roof dead load, 55 psf floor total load, and 80 plf wall load. Wall load is based on 3'-0" naximum width window or door openings

For larger openings, or multiple 3'.0" width openings spaced less than 6'-0" o.c., additional joists beneath the opening's cripple studs may be required.

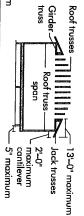
the floor span requirements for a design live load of 40 psf and dead load of 15 psf, and a live load deflection limit of L/480. Use Table applies to joists 12" to 24" o.c. that mee 12" o.c. requirements for lesser spacing.

4. For conventional roof construction using a ridge beam, the Roof Truss Span column above is equivalent to the distance between

When the roof is framed using a ridge board, the Roof Truss Span is equivalent to the distance between the supporting walls as if a the supporting wall and the ridge beam. truss is used.

5. Cantilevered joists supporting girder trusses or roof beams may require additional reinforcing.

	callinovol.	requirements at	reinforcement	below for NI	000 1000
· ·	I		span	Roof truss	
	5" maximum	cantilever	maximum	√ 2'-0"	7
	3	H	truss	Girder -	·
ı	ĺ	H		'	L



trusses running parallel to the cantilevered floor joists, the I-joist reinforcement requirements for a span of For hip roofs with the jack 26 ft. shall be permitted to

# BRICK CANTILEVER REINFORCEMENT METHODS ALLOWED

161 161	7	11.27.8%	9 	JOIST DEPTH (in.)
2882 2882 2883	26842288 8682288	28 32 32 34 34 34	28 30 32 34	ROOF TRUSS SPAN (f)
-ZZZZZZZZ	zzzz	zzz	2227-2	ال الــــــــــــــــــــــــــــــــــ
מאמאמים===	-במטטטטע	*********	×××××	= 30 psf, IOIST SPAI
aaaaxxxx	××××××1		*****	DL = 15 CING (in. 19.2
******	*****	(××××××	×××××	psf ) 24
zzzz	10-2-2-2-Z	222111	ผู้สุดสุด	ROOF [   L  =  J(  12
	******	*****	×××××	OADING = 40 pst, DIST SPAC 16
****	××××××	*****	×××××	(UNFAC DL = 15 DING (in.
****	*****	××××××	*****	(ORED) psf ) 24
100 Z		××6666	××××\	ਹ = 1.
*******	××××××	******	<×××××	= 50 psf, DIST SPA(
****	****	×××××××	·×××××	DL = 15 CING (in.
*****	****	××××××	<×××××	.psf ) 24

# INSTALLING THE GLUED FLOOR SYSTEM

- 1. Wipe any mud, dirt, water, or ice from I-joist flanges before gluing.
- 2. Snap a chalk line across the I-joists four feet in from the wall for panel edge alignment and as a boundary for spreading glue.
- 3. Spread only enough glue to lay one or two panels at a time, or follow specific recommendations from the glue manufacturer.
- 4. Lay the first panel with tongue side to the wall, and nail in place. This protects the tongue of the next panel from damage when tapped into place with a block and sledgehammer.
- 5. Apply a continuous line of glue (about 1/4-inch diameter) to the top flange of a single 1-joist. Apply glue in a winding pattern on wide areas, such as with double I-joists.
- 6. Apply two lines of glue on Lioists where panel ends butt to assure proper gluing of each end.
- 7. After the first row of panels is in place, spread glue in the groove of one or two panels at a time before laying the next row. Glue line may be continuous or spaced, but avoid squeeze-out by applying a thinner line (1/8 inch) than used on I-joist flanges.
- 8. Tap the second row of panels into place, using a block to protect groove edges.
- 9. Stagger end joints in each succeeding row of panels. A 1/8-inch space between all end joints and nail to assure accurate and consistent spacing.) /8-inch at all edges, including T&G edges, is recommended. (Use a spacer tool or an 2-1/2" common
- 10. Complete all nailing of each panel before glue sets. Check the manufacturer's recommendations for cure time. (Warm weather accelerates glue setting.) Use 2" ring- or screw-shank nails for panels 3/4-inch thick or less, and 2-1/2" ring- or screw-shank nails for thicker panels. Space nails per the finished deck can be walked on right away and will carry construction loads without damage to the table below. Closer nail spacing may be required by some codes, or for diaphragm construction. The

# FASTENERS FOR SHEATHING AND SUBFLOORING(1)

	14	20		Maximum Joist Spacing (in.)
ACTE STREET	3/4	5/8	5/8	Minimum Panel Thickness (in.)
	2	2"	2"	Common Wire or Spiral Nails
	1-3/4"	1-3/4"	1-3/4*	ail Size and Ty Ring Thread Nails or Screws
	2"	2"	2"	pe Staples
,	, n	6	6,	Maximun of Fas Edges
1.2	12	12"	12"	n Spacing feners Interm. Supports

- 1. Fasteners of sheathing and subflooring shall conform to the above table.
- 2. Staples shall not be less than 1/16-inch in diameter or thickness, with not less than a 3/8-inch crown driven with the crown parallel to framing.
- . Flooring screws shall not be less than 1/8-inch in diameter.
- 4. Special conditions may impose heavy traffic and concentrated loads that require construction in excess of the minimums shown.
- 5. Use only adhesives conforming to CAN/CGSB-71.26 Standard, Adhesives for Field-Gluing Plywood to Lumber Framing for Floor System, applied in accordance with the manufacturer's recommendations. If OSB panels with sealed surfaces and edges are to be used, use only solvent-based glues; check with
- Ref.: NRC-CNRC, National Building Code of Canada 2010, Table 9.23.3.5

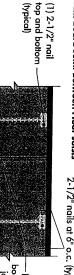
### IMPORTANT NOTE:

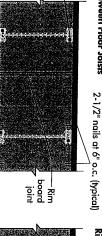
Floor sheathing must be field glued to the I-joist flanges in order to achieve the maximum spans shown in this document. If sheathing is nailed only, I-joist spans must be verified with

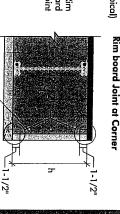
# RIM BOARD INSTALLATION DETAILS

# (8a) ATTACHMENT DETAILS WHERE RIM BOARDS ABUT

Rim board Joint Between Floor Joists

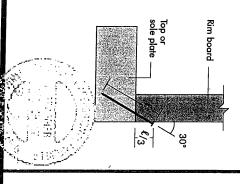






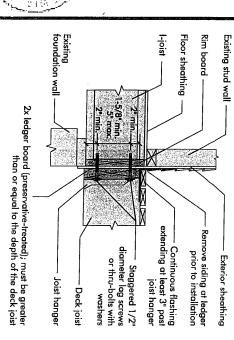
### **(P** TOE-NAIL CONNECTION AT RIM BOARD

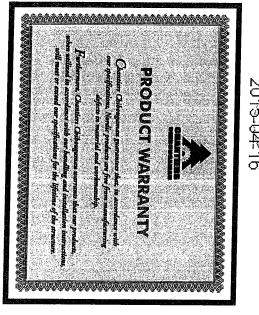
2-1/2" toe-nails at 6" o.c. (typical) —

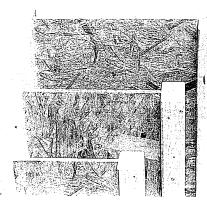


## 6 2X LEDGER TO RIM BOARD ATTACHMENT DETAIL

Rim board joint







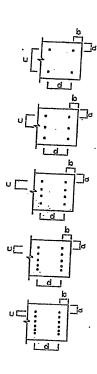
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### Engineering services inc.

TEL: (519) 287 - 2242

R.R. #1, P.O. BOX 61, GLENCOE, ONTARIO, NOL 1M0

	TIVI HEA	DED AND GO	
	LUM	BER NAILING	NVENTIONAL DETAILS
	DETAIL NUMBER	1	
	A	2.	1 12
	В	2	8
	С	2	6
	D	2	4
Compt.	1A	3	12
2	1B	3	8
	1C	3	. 6
- 1	1D	. 3:	4
	2A	4	1. 12
-	2B	4	8 .
L	2C	4	6
Ŀ	2D	4	4
L	3A	5	12
1	3B	5	. 8
L	3C	5	6
Ŀ	3D	5	4
L	4A	6	12
L	4B	6	8
Ŀ	4C	6	6
Ŀ	4D	6	4



### NOTES:

- (1) MINIMUM LUMBER EDGE DISTANCE "a" = 1"
- (2) MINIMUM LUMBER END DISTANCE "b" = 2"
- (3) MINIMUM NAIL ROW SPACING "c" = 2"
- (4) STAGGER NAILS "d/2" BETWEEN PLIES FOR MULTI-PLY MEMBERS (3 PLY OR MORE)
- (5) ALL NAILS ARE 3-1/2" ARDOX SPIRAL NAILS
- (6) DO NOT USE AIR-DRIVEN NAILS



DNO NO TÄMPICOI. 14
STRUCTURAL
COMPONENT ONLY
TO BE USED ONLY
WITH BEAM CALCS
BEARING THE
STAMP BELOWS

PROVICE NATLING DETAIL № × SEE ONO #TANN1001-14