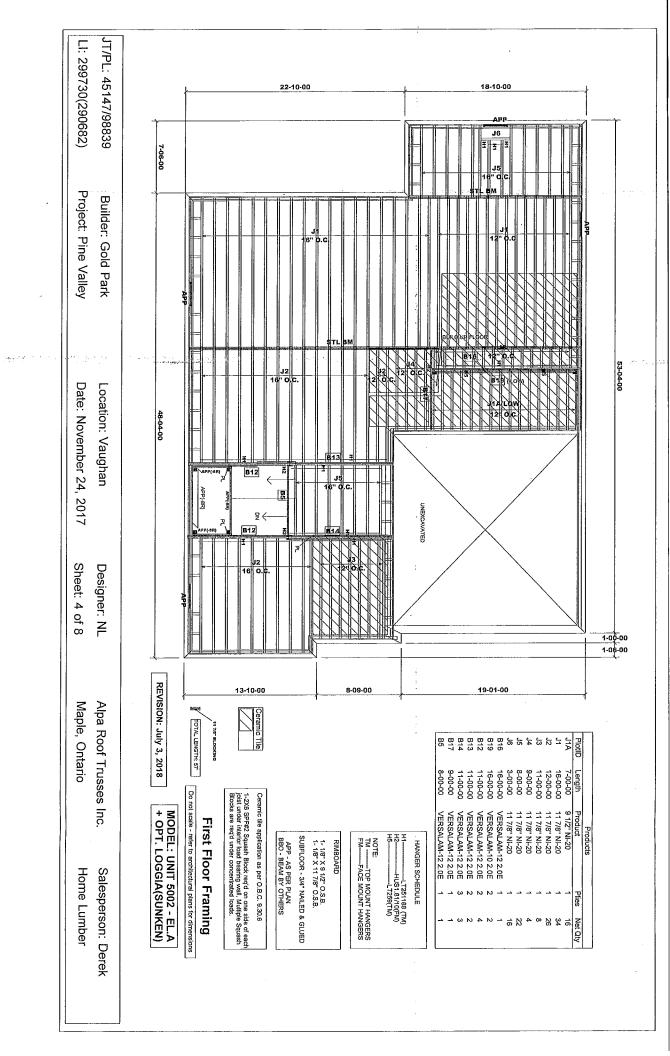
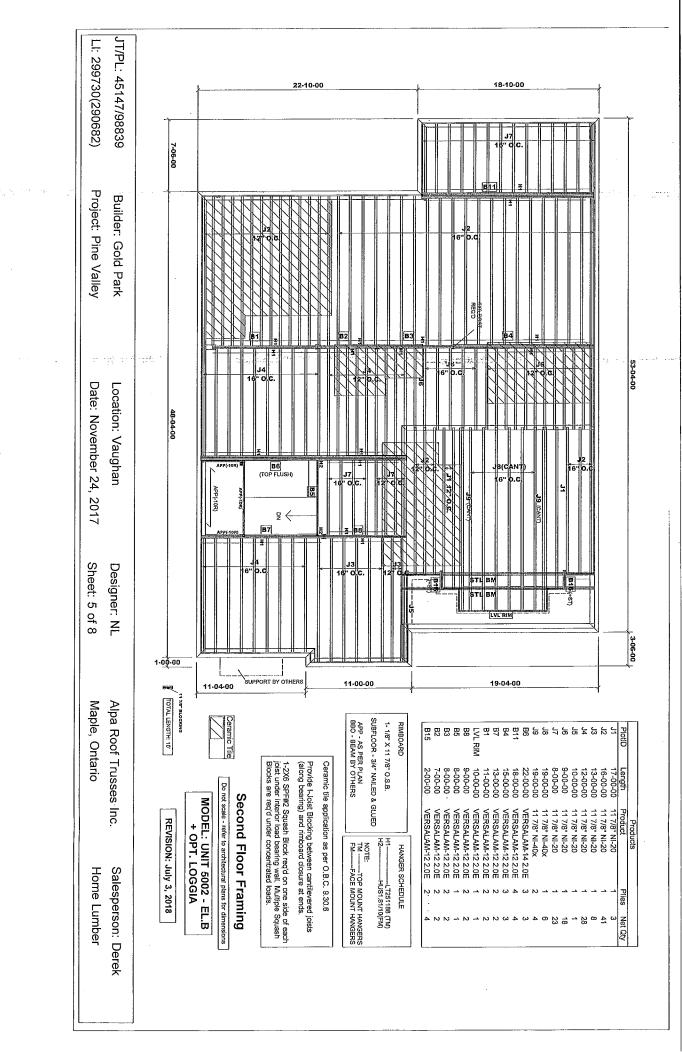
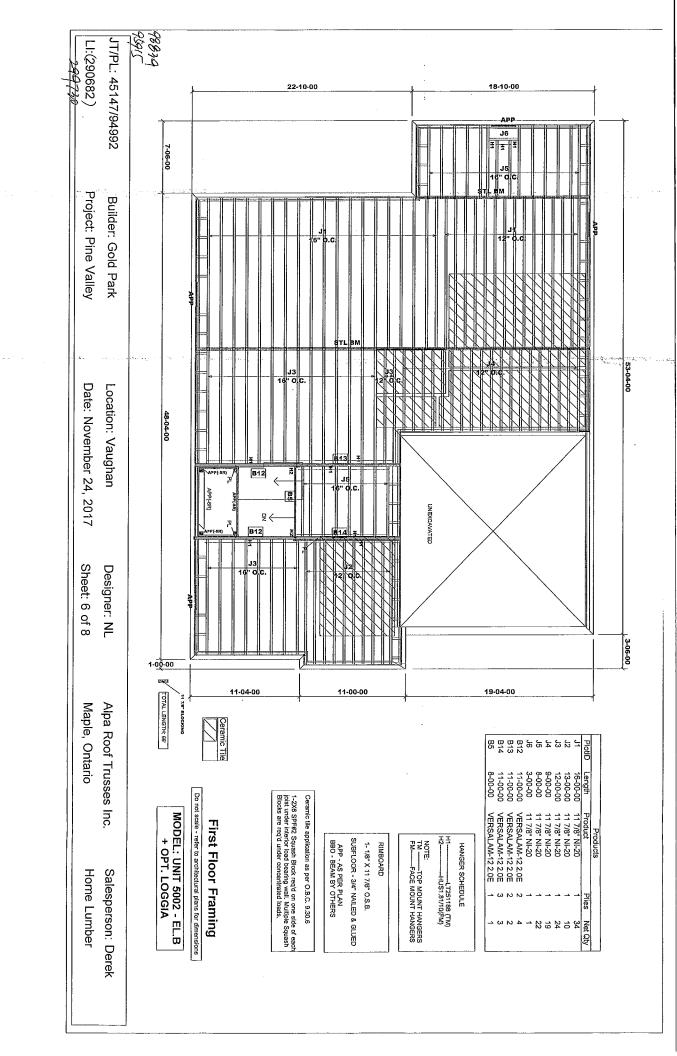


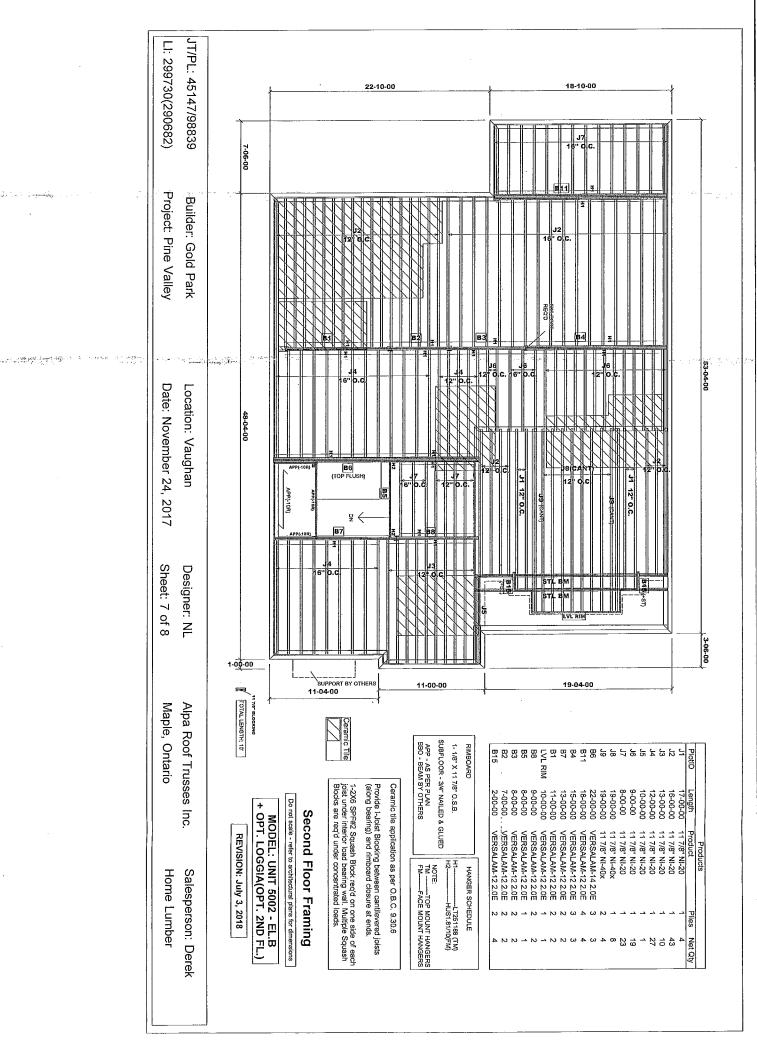
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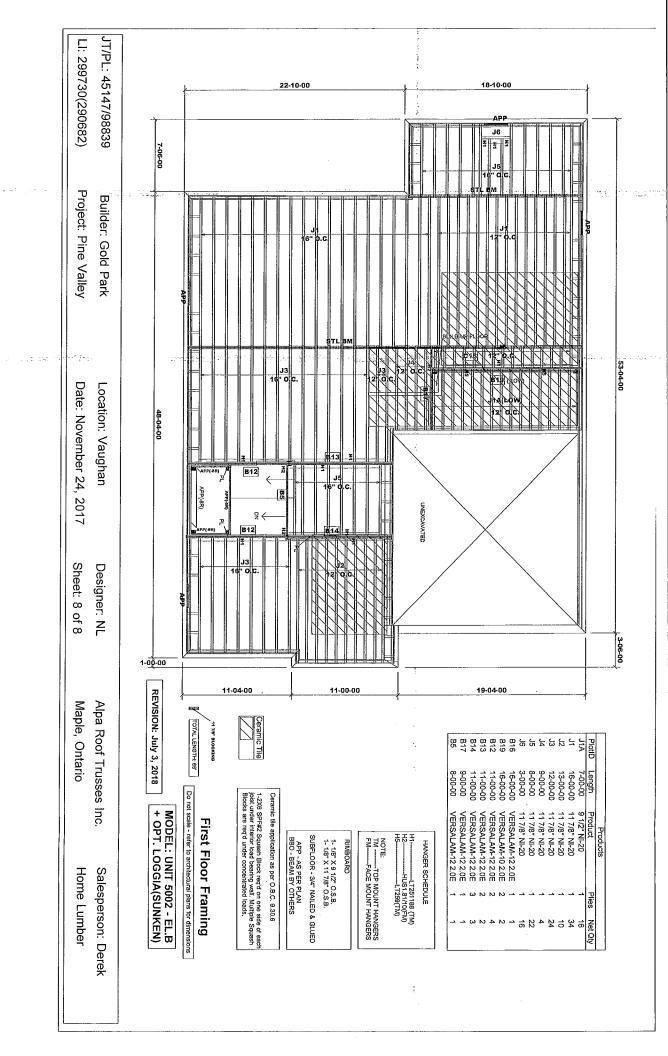






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Floor Beam\B01

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 13:14:01

BC CALC® Design Report



Build 6080

Name: Address:

45147 (5002)

Customer:

Pine Valley City, Province, Postal Code: Vaughan, ON Gold Park

Code reports:

CCMC 12472-R

File Name: 290682.bcc

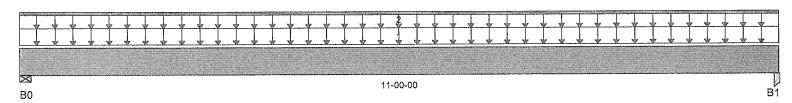
Description: Second Floor Framing

Specifier:

NL Designer:

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 11-00-00

Reaction Summary (Down / Uplift) (lbs) Wind Snow Bearing Live Dead 3,018 / 0 1,907 / 0 B0, 3-1/2" 2,995 / 0 1,892 / 0 B1, 3"

Load Summary				Live	Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End	1.00	0.65	1.00 1.15	
1	Unf. Area (lb/ft^2)	L 00-00-00	11-00-00	40	20		13-08-00
2	Unf. Lin. (lb/ft)	L 00-00-00	11-00-00		60		n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	17,525 ft-lbs	35,392 ft-lbs	49.5%	1	05-06-04
End Shear	5,307 lbs	14,464 lbs	36.7%	1	01-03-06
Total Load Defl.	L/493 (0.258")	0.529"	48.7%	4	05-06-04
Live Load Defl.	L/804 (0.158")	0.353"	44.8%	5	05-06-04
Max Defl.	0.258"	1"	25.8%	4	05-06-04
Span / Depth	10.7	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bearir	ng Supports	Dim. (L x W)		Resistance Support	Resistance Member	Material
B0	Wall/Plate	3-1/2" x 3-1/2"	6,910 lbs	91.7%	46.2%	Spruce Pine Fir
B1	Post	3" x 3-1/2"	6,858 lbs	37.7%	53.5%	Spruce Pine Fir

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 ½" spiral nails @ 10 "





Floor Beam\B02

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 13:14:56

BC CALC® Design Report



P=14 6080 Vame: Address:

45147 (5002) Pine Valley

Customer:

City, Province, Postal Code: Vaughan, ON Gold Park

Code reports:

CCMC 12472-R

File Name: 290682.bcc

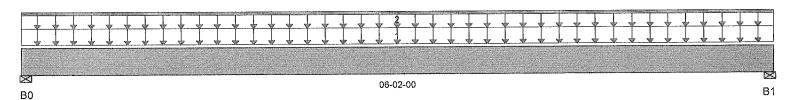
Description: Second Floor Framing

Specifier:

Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 06-02-00

Reaction Summary (Down / Uplift) (lbs)							
Bearing	Live	Dead	Snow	Wind			
B0, 3"	1,686 / 0	1,065 / 0					
B1, 3"	1,686 / 0	1,065 / 0					

Load Summary			Live	e Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End 1.00	0 0.65	1.00 1.15	
1	Unf. Area (lb/ft^2)	L 00-00-00	06-02-00 40	20		13-08-00
2	Unf. Lin. (lb/ft)	L 00-00-00	06-02-00	60		n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	5,248 ft-lbs	35,392 ft-lbs	14.8%	1	03-01-00
End Shear	2,308 lbs	14,464 lbs	16%	1	01-02-14
Total Load Defl.	L/999 (0.023")	n/a	n/a	4	03-01-00
Live Load Defl.	L/999 (0.014")	n/a	n/a	5	03-01-00
Max Defl.	0.023"	n/a	n/a	4	03-01-00
Span / Depth	5.9	n/a	n/a		00-00-00
Squash Blocks	Valid				

Beari	ng Supports	Dim. (L x W)	Demand	Resistance Support	Resistance Member	Material
B0	Wall/Plate	3" x 3-1/2"	3,859 lbs	59.7%	30.1%	Spruce Pine Fir
B1	Wall/Plate	3" x 3-1/2"	3,859 lbs	59.7%	30.1%	Spruce Pine Fir

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 ½" spiral nails @ 10" o.c, staggered in 2 rows





Floor Beam\B03

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 13:15:56

BC CALC® Design Report



Build 6080

Name: 45147 (5002) Audress:

Customer:

Pine Valley City, Province, Postal Code: Vaughan, ON

Code reports:

Gold Park CCMC 12472-R File Name: 290682.bcc

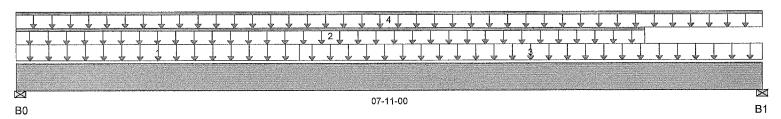
Description: Second Floor Framing

Specifier:

Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 07-11-00

Reaction Summary (Down / Uplift) (lbs)							
Bearing	Live	Dead	Snow	Wind			
B0, 3"	1,974 / 0	1,510 / 0					
B1, 2"	1,665 / 0	1,280 / 0					

Load Summary				Live	Dead	Snow	Wind	Trib.
Tag Description	Load Type	Ref. Start	End	1.00	0.65 1.00 1.15			
1	Unf. Area (lb/ft^2)	L 00-00-00	03-00-00	40	20			13-08-00
7	Unf. Lin. (lb/ft)	L 00-00-00	06-08-00		60			n/a
	Unf. Area (lb/ft^2)	L 03-00-00	07-11-00	40	20			10-02-00
4	Unf. Lin. (lb/ft)	L 00-00-00	07-11-00		60			n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	8,055 ft-lbs	35,392 ft-lbs	22.8%	1	03-09-10
End Shear	3,204 lbs	14,464 lbs	22.2%	1	01-02-14
Total Load Defl.	L/999 (0.062")	n/a	n/a	4	03-11-11
Live Load Defl.	L/999 (0.035")	n/a	n/a	5	03-11-11
Max Defl.	0.062"	n/a	n/a	4	03-11-11
Span / Depth	7.7	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ring Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	3" x 3-1/2"	4,848 lbs	75.1%	37.8%	Spruce Pine Fir
B1	Wall/Plate	2" x 3-1/2"	4,098 lbs	95.2%	48%	Spruce Pine Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

O86.

Design based on Dry Service Condition.

ortance Factor: Normal Part code: Part 4

o.c, staggered in 2 rows

3 ½" spiral nails @ (1)

Nail one ply to another with



Floor Beam\B04

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 13:17:42

BC CALC® Design Report



File Name: 290682.bcc

Description: Second Floor Framing

Specifier: Designer: NL

Company: Alpa Roof Trusses

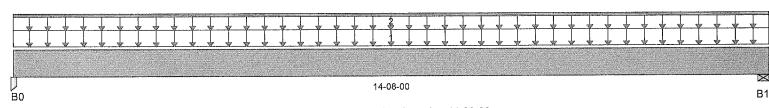
Misc:

45147 (5002) Name: Address: Pine Valley City, Province, Postal Code: Vaughan, ON Customer: Gold Park

Code reports:

Build 6080

CCMC 12472-R



Total Horizontal Product Length = 14-08-00

Reaction Summary (Down / Uplift) (lbs)								
Bearing	Live	Dead	Snow	Wind				
B0, 2"	3,538 / 0	2,337 / 0						
B1. 3-1/2"	3,599 / 0	2.377 / 0						

Load Summary				Live	Dead Snow Wind		Trib.
Tag Description	Load Type	Ref. Start	End	1.00	0.65	1.00 1.15	
1	Unf. Area (lb/ft^2)	L 00-00-00	14-08-00	40	20		12-02-00
2	Unf. Lin. (lb/ft)	L 00-00-00	14-08-00		60		n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	29,064 ft-lbs	55,212 ft-lbs	52.6%	1	07-03-04
End Shear	6,920 lbs	21,696 lbs	31.9%	1	01-01-14
Total Load Defl.	L/328 (0.524")	0.717"	73.1%	4	07-03-04
Live Load Defl.	L/545 (0.315")	0.478"	66%	5	07-03-04
Max Defl.	0.524"	1"	52.4%	4	07-03-04
Span / Depth	14.5	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ing Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Post	2" x 5-1/4"	8,229 lbs	45.2%	64.2%	Spruce Pine Fir
B1	Wall/Plate	3-1/2" x 5-1/4"	8,370 lbs	74%	37.3%	Spruce Pine Fir

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 ½" spiral nails @ 6" o.c, staggered in 2 rows





Floor Beam\B05

BC CALC® Design Report



Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 13:25:00

Build 6080

Name:

45147 (5002)

Pine Valley Audress: City, Province, Postal Code: Vaughan, ON

Customer:

Gold Park

Code reports:

CCMC 12472-R

File Name: 290682.bcc

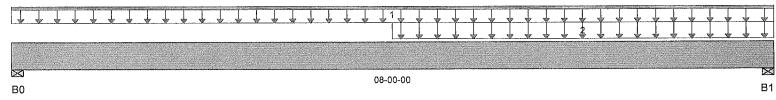
Description: Second Floor Framing

Specifier:

NL Designer:

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 08-00-00

Reaction Summary (Down / Uplift) (lbs)							
Bearing	Live	Dead	Snow	Wind			
B0, 3-1/2"	278 / 0	144 / 0					
B1, 3-1/2"	658 / 0	286 / 0					

Load Summary			Live	Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End 1.00	0.65	1.00 1.15	
1	Unf. Lin. (lb/ft)	L 00-00-00	08-00-00 27	14		n/a
2	Unf. Area (lb/ft^2)	L 04-00-00	08-00-00 40	15		04-06-00

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	1,859 ft-lbs	17,696 ft-lbs	10.5%	1	04-09-03
End Shear	808 lbs	7,232 lbs	11.2%	1	06-08-10
Total Load Defl.	L/999 (0.026")	n/a	n/a	4	04-03-01
Live Load Defl.	L/999 (0.018")	n/a	n/a	5	04-03-01
Max Defl.	0.026"	n/a	n/a	4	04-03-01
Span / Depth	7.6	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bearing Supports	Dim. (L x W)	Demand	Resistance Support	Resistance Member	Material E
B0 Wall/Plate	3-1/2" x 1-3/4"	596 lbs	15.8%	8%	Spruce Pine Fir
B1 Wall/Plate	3-1/2" x 1-3/4"	1,346 lbs	35.7%	18%	Spruce Pine Fir

Disclosure

Completeness and accuracy of input must be verified by anyone who would rely on output as evidence of suitability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

BC CALC®, BC FRAMER®, AJS™ ALLJOIST®, BC RIM BOARD™, BCI®, BOISE GLULAM™, SIMPLE FRAMING SYSTEM®, VERSA-LAM®, VERSA-RIM PLUS®, VERSA-RIM®, VERSA-STRAND®, VERSA-STUD® are trademarks of Boise Cascade Wood

Products L.L.C.

er eller PROFESSION

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4



Triple 1-3/4" x 14" VERSA-LAM® 2.0 3100 SP

Floor Beam\B06

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 15:41:14

BC CALC® Design Report



Build 6080

Vame: Audress:

45147 (5002) Pine Valley

City, Province, Postal Code: Vaughan, ON Customer:

Gold Park

Code reports:

CCMC 12472-R

File Name: 290682.bcc

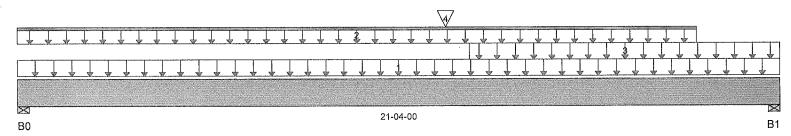
Description: Second Floor Framing

Specifier:

Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 21-04-00

		Total Fronzontar 1	oddot zotigin z t	0,00			
Reaction Summary (Down / Uplift) (lbs)							
Bearing	Live	Dead	Snow	Wind			
B0, 3-1/2"	2,954 / 0	2,306 / 0					
B1. 3-1/2"	3,831 / 0	2,512 / 0					

Load Summary				Live	Dead	Snow	Wind	Trib.
Tag Description	Load Type	Ref. Start	End	1.00	0.65	1.00	1.15	
	Unf. Area (lb/ft^2)	L 00-00-00	21-04-00	40	20			06-00-00
	Unf. Lin. (lb/ft)	L 00-00-00	19-00-00		60			n/a
3	Unf. Area (lb/ft^2)	L 12-08-00	21-04-00	40	15			04-00-00
4	Conc. Pt. (lbs)	L 12-00-00	12-00-00	278	144			n/a

	Factored	Factored	Demand /	Load	Location
Controls Summary	Demand	Resistance	Resistance	Case	
Pos. Moment	42,064 ft-lbs	75,349 ft-lbs	55.8%	1	12-00-00
End Shear	7,644 lbs	25,578 lbs	29.9%	. 1	19-10-08
Total Load Defl.	L/257 (0.976")	1.044"	93.5%	4	10-08-03
Live Load Defl.	L/444 (0.564")	0.696"	81%	5	11-00-02
Max Defl.	0.976"	1"	97.6%	4	10-08-03
Span / Depth	17.9	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ing Supports	Dim. (L x W)	Demand	Resistance Support	Resistance Member	Material	
B0	Wall/Plate	3-1/2" x 5-1/4"	7,313 lbs	64.7%	32.6%	Spruce Pine Fir	ſ
B1	Wall/Plate	3-1/2" x 5-1/4"	8,886 lbs	78.6%	39.6%	Spruce Pine Fir	٢

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

gn based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 ½" spiral nails @ LO!





Floor Beam\B07

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 14:32:51

BC CALC® Design Report



Build 6080

Audress:

45147 (5002)

City, Province, Postal Code: Vaughan, ON

Name:

Pine Valley

Customer: Code reports: Gold Park

CCMC 12472-R

File Name: 290682.bcc

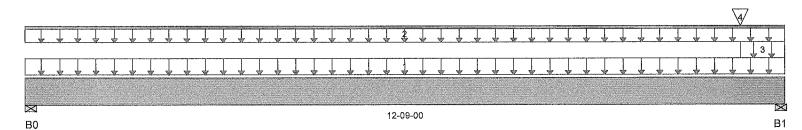
Description: Second Floor Framing

Specifier:

Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 12-09-00

Total Horizontal House acing (i)								
Reaction Summary (Down / Uplift) (Ibs)								
Bearing	Live	Dead	Snow	Wind				
B0, 3-1/2"	1,610 / 0	1,264 / 0						
B1, 3"	2,313 / 0	1,573 / 0						

Load Summary					Live	Dead	Snow	Wind	Trib.
Tag Description	Load Type	Ref. S	Start E	nd	1.00	0.65	1.00	1.15	
	Unf. Area (lb/ft^2)	L 00-)-00-00 1	2-09-00	40	20			06-02-00
	Unf, Lin. (lb/ft)	L 00)-00-00 1	2-09-00		60			n/a
3	Unf. Area (lb/ft^2)	L 12	2-00-00 1	2-09-00	40	20			04-00-00
4	Conc. Pt. (Ìbs)	L 12	2-00-00 1	2-00-00	658	286			n/a

	Factored	Factored	Demand /	Load	Location
Controls Summary	Demand	Resistance	Resistance	Case	
Pos. Moment	12,086 ft-lbs	35,392 ft-lbs	34.1%	1	06-06-11
End Shear	3,925 lbs	14,464 lbs	27.1%	1	11-06-02
Total Load Defl.	L/604 (0.245")	0.617"	39.7%	4	06-04-12
Live Load Defl.	L/1,072 (0.138") 0.411"	33.6%	5	06-04-12
Max Defl.	0.245"	1"	24.5%	4	06-04-12
Span / Depth	12.5	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ing Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	3-1/2" x 3-1/2"	3,994 lbs	53%	26.7%	Spruce Pine Fir
B1	Wall/Plate	3" x 3-1/2"	5,436 lbs	84.2%	42.4%	Spruce Pine Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

gn based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 ½" spiral nails @ (Zyl o.c, staggered in 2 rows





Floor Beam\B08

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 14:36:58

BC CALC® Design Report



Build 6080

Name: Audress:

45147 (5002) Pine Valley

City, Province, Postal Code: Vaughan, ON Customer:

Code reports:

Gold Park CCMC 12472-R File Name: 290682.bcc

Description: Second Floor Framing

Specifier:

Designer: NL

Company: Alpa Roof Trusses

Misc:

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⊠ B0			 				 							07-																I	≥≲ 1

Total Horizontal Product Length = 08-07-00

Reaction Summary (Down / Uplift) (lbs) Wind Bearing Dead Snow B0, 3" 1,623 / 0 1,119 / 0 B1, 3-1/2" 1,130 / 0 1,639 / 0

Load Summary			Live	Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End 1.00	0.65	1.00 1.15	
1	Unf. Area (lb/ft^2)	L 00-00-00	08-07-00 40	20		09-06-00
2	Unf. Lin. (lb/ft)	L 00-00-00	08-07-00	60		n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	7,483 ft-lbs	35,392 ft-lbs	21.1%	1	04-03-04
End Shear	2,721 lbs	14,464 lbs	18.8%	1	01-02-14
Total Load Defl.	L/999 (0.066")	n/a	n/a	4	04-03-04
Live Load Defl.	L/999 (0.039")	n/a	n/a	5	04-03-04
Max Defl.	0.066"	n/a	n/a	4	04-03-04
Span / Depth	8.3	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ing Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	3" x 3-1/2"	3,833 lbs	59.3%	29.9%	Spruce Pine Fir
В1	Wall/Plate	3-1/2" x 3-1/2"	3,871 lbs	51.4%	25.9%	Spruce Pine Fir

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 1/2" spiral nails @ [21





BC CALC® Design Report

Double 1-3/4" x 11-7/8" VERSA-LAM® 2.0 3100 SP

Floor Beam\B09

November 24, 2017 13:34:01

Dry | 1 span | No cantilevers | 0/12 slope (deg)

Build 6080

Name: Auuress:

45147 (5002)

Customer:

Pine Valley City, Province, Postal Code: Vaughan, ON Gold Park

Code reports:

CCMC 12472-R

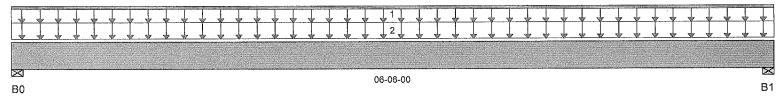
File Name: 290682.bcc

Description: Second Floor Framing

Specifier: NL Designer:

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 06-06-00

Reaction Summary (Down / Uplift) (lbs)											
Bearing	Live	Dead	Snow	Wind							
B0, 3-1/2"	88 / 0	892 / 0	921 / 0								
B1, 3-1/2"	88 / 0	892 / 0	921 / 0 -								

Load Summary				Live	Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End	1.00	0.65	1.00 1.15	
1	Unf. Lin. (lb/ft)	L 00-00-00	06-06-00	27	114		n/a
2	Unf. Area (lb/ft^2)	L 00-00-00	06-06-00		11	21	13-06-00

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	3,568 ft-lbs	35,392 ft-lbs	10.1%	5	03-03-00
End Shear	1,539 lbs	14,464 lbs	10.6%	5	01-03-06
Total Load Defl.	L/999 (0.017")	n/a	n/a	13	03-03-00
Live Load Defl.	L/999 (0.008")	n/a	n/a	17	03-03-00
Max Defl.	0.017"	n/a	n/a	13	03-03-00
Span / Depth	6.1	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ing Supports	Dim. (L. x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
В0	Wall/Plate	3-1/2" x 3-1/2"	2,541 lbs	33.7%	17%	Spruce Pine Fir
B1	Wall/Plate	3-1/2" x 3-1/2"	2,541 lbs	33.7%	17%	Spruce Pine Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 1/2" spiral nails @ 12" o.c, staggered in 2 rows





BC CALC® Design Report

Double 1-3/4" x 11-7/8" VERSA-LAM® 2.0 3100 SP

Floor Beam\B10

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 15:16:07

Build 6080

Name: Audress:

45147 (5002)

Customer:

Pine Valley City, Province, Postal Code: Vaughan, ON Gold Park

Code reports:

CCMC 12472-R

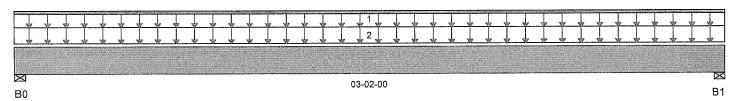
File Name: 290682.bcc

Description: Second Floor Framing

Specifier: Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 03-02-00

Reaction Summary (Down / Uplift) (lbs) Wind Snow Bearing Dead 348 / 0 283/0 B0, 3-1/2" 43 / 0 43 / 0 348 / 0 283 / 0 B1, 3-1/2"

Load Summary			L	Live	Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End 1	1.00	0.65	1.00 1.15	
1	Unf. Lin. (lb/ft)	L 00-00-00	03-02-00 2	27	114		n/a
2	Unf. Area (lb/ft^2)	L 00-00-00	03-02-00		11	21	08-06-00

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	509 ft-lbs	35,392 ft-lbs	1.4%	5	01-07-00
End Shear	168 lbs	14,464 lbs	1.2%	5	01-03-06
Total Load Defl.	L/999 (0")	n/a	n/a	13	01-07-00
Live Load Defl.	L/999 (0")	n/a	n/a	17	01-07-00
Max Defl.	0"	n/a	n/a	13	01-07-00
Span / Depth	2.7	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bearii	ng Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wali/Plate	3-1/2" x 3-1/2"	880 lbs	11.7%	5.9%	Spruce Pine Fir
B1	Wall/Plate	3-1/2" x 3-1/2"	880 lbs	11.7%	5.9%	Spruce Pine Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 1/2" spiral nails @ 6"





Floor Beam\B11

BC CALC® Design Report



Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 14:37:00

Build 6080

Name:

45147 (5002) Pine Valley

Augress: City, Province, Postal Code: Vaughan, ON Customer:

Code reports:

Gold Park CCMC 12472-R File Name: 290682.bcc

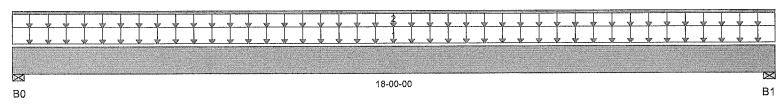
Description: Second Floor Framing

Specifier:

Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 18-00-00

Reaction Summary (D	Down / Uplift) (lbs)			
Bearing	Live	Dead	Snow	Wind
B0, 3-1/2"	4,200 / 0	2,857 / 0		
B1. 3-1/2"	4.200 / 0	2.857 / 0		

Load Summary			Live	Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End 1.00	0.65	1.00 1.15	
1	Unf. Area (lb/ft^2)	L 00-00-00	18-00-00 40	20		11-08-00
2	Unf. Lin. (lb/ft)	L 00-00-00	18-00-00	60		n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	42,185 ft-lbs	73,615 ft-lbs	57.3%	1	09-00-00
End Shear	8,466 lbs	28,927 lbs	29.3%	1	01-03-06
Total Load Defl.	L/246 (0.855")	0.877"	97.5%	4	09-00-00
Live Load Defl.	L/414 (0.509")	0.585"	87%	5	09-00-00
Max Defl.	0.855"	1"	85.5%	4	09-00-00
Span / Depth	17.7	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ing Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	3-1/2" x 7"	9,871 lbs	65.5%	33%	Spruce Pine Fir
B1	Wall/Plate	3-1/2" x 7"	9,871 lbs	65.5%	33%	Spruce Pine Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

Design based on Dry Service Condition.

Importance Factor : Normal Part code : Part 4

Nail one ply to another with 3 ½" spiral nails @ 6"

o.c. staggered in 2 rows , bus 1/2

NUTS of WASHERLS @ 2013





Floor Beam\B12

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 14:39:03

BC CALC® Design Report

Build 6080 45147 (5002) Name:

Augress: Pine Valley City, Province, Postal Code: Vaughan, ON

Customer:

Gold Park

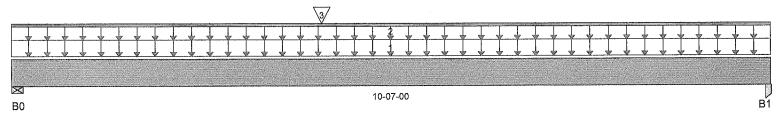
Code reports: CCMC 12472-R File Name: 290682.bcc

Description: First Floor Framing

Specifier: Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 10-07-00

Reaction Summary (Down / Uplift) (lbs)					
Bearing	Live	Dead	Snow	Wind	
B0, 3-1/2"	2,014 / 0	1,138 / 0			
B1, 3"	1,787 / 0	1,050 / 0			

Load Summary				Live	Dead	Snow	Wind	Trib.
Tag Description	Load Type	Ref. Start	End	1.00	0.65	1.00	1.15	
1	Unf. Area (lb/ft^2)	L 00-00-00	10-07-00	40	15			06-04-00
Production of the second	Unf. Lin. (lb/ft)	L 00-00-00	10-07-00		60			n/a
	Conc. Pt. (lbs)	L 04-04-00	04-04-00	1,120	420			n/a

Canduala Comencana	Factored	Factored	Demand /	Load	Location
Controls Summary	Demand	Resistance	Resistance	Case	
Pos. Moment	12,721 ft-lbs	35,392 ft-lbs	35.9%	1	04-04-00
End Shear	3,688 lbs	14,464 lbs	25.5%	1	01-03-06
Total Load Defl.	L/762 (0.16")	0.508"	31.5%	4	05-03-05
Live Load Defl.	L/999 (0.104")	n/a	n/a	5	05-01-06
Max Defl.	0.16" `	1"	16%	4	05-03-05
Span / Depth	10.3	n/a	n/a		00-00-00
Squash Blocks	Valid				

Beari	ng Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	3-1/2" x 3-1/2"	4,443 lbs	59%	29.7%	Spruce Pine Fir
B1	Post	3" x 3-1/2"	3,994 lbs	21.9%	31.2%	Spruce Pine Fir

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

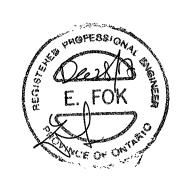
Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 1/2" spiral nails @ (2."





Floor Beam\B13

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 15:16:21

BC CALC® Design Report

Build 6080 Name:

Audress:

45147 (5002)

Customer:

Pine Valley City, Province, Postal Code: Vaughan, ON

Code reports:

Gold Park CCMC 12472-R File Name: 290682.bcc

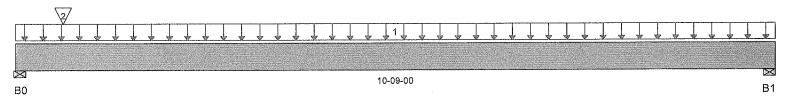
Description: First Floor Framing

Specifier:

Designer:

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 10-09-00

Reaction Summary (Down / Uplift) (lbs)						
Bearing	Live	Dead	Snow	Wind		
B0, 3"	2,873 / 0	1,425 / 0				
B1, 3-1/2"	2,194 / 0	1,158 / 0				

Load Summary			Live	Dead	Snow Wind	Trib,
Tag Description	Load Type	Ref. Start	End 1.00	0.65	1.00 1.15	
1	Unf. Area (lb/ft^2)	L 00-00-00	10-09-00 40	20		10-00-00
2	Conc. Pt. (lbs)	L 00-08-00	00-08-00 767	304		n/a

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	11,914 ft-lbs	35,392 ft-lbs	33.7%	1	05-02-11
End Shear	4,133 lbs	14,464 lbs	28.6%	1	01-02-14
Total Load Defl.	L/744 (0.167")	0.517"	32.3%	4	05-04-04
Live Load Defl.	L/999 (0.109")	n/a	n/a	5	05-04-04
Max Defl.	0.167"	1"	16.7%	4	05-04-04
Span / Depth	10.4	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ring Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	3" x 3-1/2"	6,091 lbs	94.3%	47.5%	Spruce Pine Fir
В1	Wall/Plate	3-1/2" x 3-1/2"	4,739 lbs	62.9%	31.7%	Spruce Pine Fir

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 1/2" spiral nails @ 121





Build 6080

Auuress:

Customer:

Code reports:

Vame:

Triple 1-3/4" x 11-7/8" VERSA-LAM® 2.0 3100 SP

Floor Beam\B14

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 15:16:32

BC CALC® Design Report

City, Province, Postal Code: Vaughan, ON



45147 (5002)

Pine Valley

File Name: 290682.bcc

Description: First Floor Framing

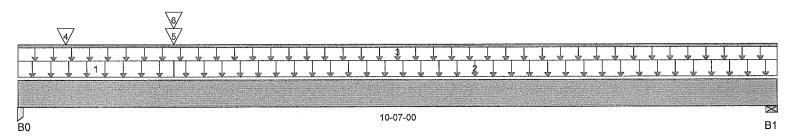
Specifier:

Designer: NL

Company: Alpa Roof Trusses

Gold Park CCMC 12472-R

Misc:



Total Horizontal Product Length = 10-07-00

Reaction Summary (Dov	vn / Uplift) (lbs)				
Bearing	Live	Dead	Snow	Wind	
B0, 3"	5,509 / 0	3,723 / 0			
B1, 3-1/2"	2,754 / 0	1,931 / 0			

Load Summary					Live	Dead	Snow	Wind	Trib.
Tag Description	Load Type	Re	f. Start	End	1.00	0.65	1.00	1.15	
	Unf. Area (lb/ft^2)	L	00-00-00	02-02-00	40	20		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	10-00-00
	Unf. Area (lb/ft^2)	<u></u>	02-02-00	10-07-00	40	20			09-03-00
3	Unf. Lin. (lb/ft)	L	00-00-00	10-07-00		60			n/a
4	Conc. Pt. (lbs)	L.	00-08-00	00-08-00	346	146			n/a
5	Conc. Pt. (lbs)	L	02-02-00	02-02-00	2,313	1,573			n/a
6	Conc. Pt. (lbs)	L	02-02-00	02-02-00	1,623	1,119			n/a

	Factored	Factored	Demand /	Load	Location
Controls Summary	Demand	Resistance	Resistance	Case	
Pos. Moment	22,752 ft-lbs	55,212 ft-lbs	41.2%	1	03-02-01
End Shear	11,337 lbs	21,696 lbs	52.3%	1	01-02-14
Total Load Defl.	L/604 (0.202")	0.508"	39.8%	4	04-11-07
Live Load Defl.	L/999 (0.119")	n/a	n/a	5	04-11-07
Max Defl.	0.202"	1"	20.2%	4	04-11-07
Span / Depth	10.3	n/a	n/a		00-00-00
Squash Blocks	Valid				

Beari	ng Supports	Dim. (L x W)	Demand	Resistance Support	Resistance Member	Material
B0	Post	3" x 5-1/4"	12,918 lbs	47.3%	67.2%	Spruce Pine Fir
B1	Wall/Plate	3-1/2" x 5-1/4"	6,544 lbs	57.9%	29.2%	Spruce Pine Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Posistance Factor phi has been applied to all presented results per CSA O86.

CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

O₆6.

Design based on Dry Service Condition.

Importance Factor : Normal Part code : Part 4

Nail one ply to another with 3 $\frac{1}{2}$ " spiral nails @ $\binom{0}{4}$





Floor Beam\B15

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 16:26:13

Build 6080

BC CALC® Design Report

45147 (5002)

Pine Valley City, Province, Postal Code: Vaughan, ON

Customer: Code reports:

Auuress:

Jame:

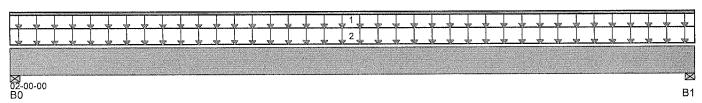
Gold Park CCMC 12472-R File Name: 290682.bcc

Description: Second Floor Framing

Specifier: Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 02-00-00

Reaction Summary (Down / Uplift) (lbs)							
Bearing	Live	Dead	Snow	Wind			
B0, 3-1/2"	27 / 0	170 / 0	84 / 0				
B1, 3-1/2"	27 / 0	170 / 0	84 / 0				

Load Summary			Liv	ve Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End 1.0	0.65	1.00 1.15	
1	Unf. Lin. (lb/ft)	L 00-00-00	02-00-00 27	' 114		n/a
2	Unf. Area (lb/ft^2)	L 00-00-00	02-00-00	11	21	04-00-00

Controls Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	71 ft-lbs	23,005 ft-lbs	0.3%	0	01-00-00
End Shear	67 lbs	9,401 lbs	0.7%	0	01-03-06
Span / Depth	1.6	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ring Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material
B0	Wall/Plate	3-1/2" x 3-1/2"	238 lbs	4.9%	2.5%	Spruce Pine Fir
B1	Wall/Plate	3-1/2" x 3-1/2"	238 lbs	4.9%	2.5%	Spruce Pine Fir

Notes

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Nail one ply to another with 3 1/2" spiral nails @ 611 o.c, staggered in 2 rows





Floor Beam\B16

BC CALC® Design Report



Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 16:26:58

Build 6080

Name:

45147 (5002)

Auuress: Pine Valley City, Province, Postal Code: Vaughan, ON

Customer:

Gold Park

Code reports:

CCMC 12472-R

File Name: 290682.bcc

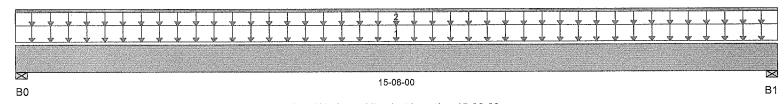
Description: First Floor Framing

Specifier:

Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 15-06-00

Reaction Summary (Down / Uplift) (lbs)							
Bearing	Live	Dead	Snow	Wind			
B0, 3-1/2"	465 / 0	744 / 0					
B1, 3-1/2"	465 / 0	744 / 0					

Load Summary			Liv	re Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End 1.0	0 0.65	1.00 1.15	
1	Unf. Area (lb/ft^2)	L 00-00-00	15-06-00 40	20		01-06-00
2	Unf. Lin. (lb/ft)	L 00-00-00	15-06-00	60		n/a

ontrols Summary	Factored Demand	Factored Resistance	Demand / Resistance	Load Case	Location
Pos. Moment	5,940 ft-lbs	17,696 ft-lbs	33.6%	1	07-09-00
End Shear	1,359 lbs	7,232 lbs	18.8%	1	01-03-06
Total Load Defl.	L/491 (0.368")	0.752"	48.9%	4	07-09-00
Live Load Defl.	L/1,276 (0.141"	0.501"	28.2%	5	07-09-00
Max Defl.	0.368"	1"	36.8%	4	07-09-00
Span / Depth	15.2	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bear	ing Supports	Dim. (L x W)	Demand	Resistance Support	Resistance Member	Material E
B0 B1	Wall/Plate Wall/Plate	3-1/2" x 1-3/4" 3-1/2" x 1-3/4"	1,628 lbs 1,628 lbs	43.2% 43.2%	21.8% 21.8%	Spruce Pine Fir E
						ř.

Disclosure

Completeness and accuracy of input must be verified by anyone who would rely on output as evidence of suitability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

BC CALC®, BC FRAMER® , AJS™ ALLJOIST®, BC RIM BOARD™, BCI®, BOISE GLULAM™, SIMPLE FRAMING SYSTEM®, VERSA-LAM®, VERSA-RIM PLUS®, VERSA-RIM®, VERSA-STRAND®, VERSA-STUD® are trademarks of Boise Cascade Wood Products L.L.C.

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA O86.

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4





Floor Beam\B17

Dry | 1 span | No cantilevers | 0/12 slope (deg)

November 24, 2017 16:27:38

BC CALC® Design Report



45147 (5002) Name: Pine Valley Auuress: City, Province, Postal Code: Vaughan, ON

Customer: Code reports:

Build 6080

Gold Park CCMC 12472-R File Name: 290682.bcc

Description: First Floor Framing

Specifier: Designer: NL

Company: Alpa Roof Trusses

Misc:

	3		
<u> </u>	<u> </u>		
	 		
	Hame the state of the state of the property of the state	09-00-00	
0		08-00-00	В

Total Horizontal Product Length = 09-00-00

Reaction Summary (Down / Uplift) (lbs)									
Bearing	Live	Dead	Snow	Wind					
B0, 3-1/2"	525 / 0	943 / 0	,						
B1, 3-1/2"	248 / 0	555 / 0							

Load Summary					Live	Dead	Snow	Wind	Trib.
Tag Description	Load Type	Ref	f. Start	End	1.00	0.65	1.00	1.15	
1	Unf. Lin. (lb/ft)	L	00-00-00	09-00-00	27	74			n/a
Property Control of the Control of t	Unf. Lin. (lb/ft)	L	00-00-00	02-05-00	27	14			n/a
	Conc. Pt. (lbs)	L	02-05-00	02-05-00	465	744			n/a

	Factored	Factored	Demand /	Load	Location
Controls Summary	Demand	Resistance	Resistance	Case	
Pos. Moment	2,509 ft-lbs	11,502 ft-lbs	21.8%	0	02-05-00
End Shear	1,152 lbs	4,701 lbs	24.5%	0	01-03-06
Total Load Defl.	L/999 (0.067")	n/a	n/a	4	04-01-14
Live Load Defl.	L/999 (0.023")	n/a	n/a	5	04-01-14
Max Defl.	0.067"	n/a	n/a	4	04-01-14
Span / Depth	8.6	n/a	n/a		00-00-00
Squash Blocks	Valid				

Bearing	g Supports	Dim. (L x W)	Demand	Demand/ Resistance Support	Demand/ Resistance Member	Material	
	Wall/Plate Wall/Plate	3-1/2" x 1-3/4" 3-1/2" x 1-3/4"	1,321 lbs 776 lbs	53.9% 31.7%	27.2% 16%	Spruce F Spruce F	

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA

Design based on Dry Service Condition.

Importance Factor: Normal Part code: Part 4

Disclosure

Completeness and accuracy of input must be verified by anyone who would rely on output as evidence of sultability for particular application. Output here based on building code-accepted design properties and analysis methods. Installation of Boise Cascade engineered wood products must be in accordance with current Installation Guide and applicable building codes. To obtain Installation Guide or ask questions, please call 1-800-964-6999 before installation.

BC CALC®, BC FRAMER®, AJS™ ALLJOIST® , BC RIM BOARD $^{\text{TM}}$, BCI® , BOISE GLULAM $^{\text{TM}}$, SIMPLE FRAMING ir system®, versa-lam®, versa-rim PLUS®, VERSA-RIM®, VERSA-STRAND®, VERSA-STUD® are trademarks of Boise Cascade Wood Products L.L.C.



NORDIC **STRUCTURES**

COMPANY Nov. 24, 2017 14:35 PROJECT

45147(5002) Gold Park Pine Valley, Vaughan 1-NI-20-8'(1ST FL., under stair).wwb

Design Check Calculation Sheet

Loads:

l	Load	Type	Distribution	Pat-				Unit	
L				tern	Start	End	Start	End	
ı	Loadl	Dead	Full Area				15.00		psf
ı	Load2	Live	Full Area				40.00		psf
ı	Load3	Live	Partial UDL		0.07	3.66	160.0	160.0	plf
ı	Load4	Dead	Partial UDL		0.07	3.66	60.0	60.0	plf
l	Self-weight	Dead	Full UDL				2.4		plf

Maximum Reactions (lbs), Bearing Resistances (lbs) and Bearing Lengths (in):

	13'-7.8"	
	कि	13·6"
Unfactored:		
Dead Live	304 767	146 346
Factored: Total	1531	702
Bearing: Resistance		,
Joist	1965 2798	1965 2798
Support Des ratio		
Joist Support	0.78	0.36
Load case	#2	0.25
Length Min req'd	1-3/4	1-3/4 1-3/4
Stiffener	No	No
Kd KB support	1.00	1,00 1.00
fcp sup Kzcp sup	0.78 0.55 #2 1-3/4 1-3/4 No 1.00 1.00 769	1.00 769 1.03
Bearing for wall	supports is perpendicular-to-grain bearing on top plate. No stud design included.	1,03

Nordic 11-7/8" NI-20 Floor joist @ 12" o.c. Supports: All - Lumber Wall, No.1/No.2 Total length: 13'-7.8"; 3/4" nailed and glued OSB sheathing This section PASSES the design code check.

Limit States Design using CSA O86-14 and Vibration Criterion:

Criterion	Analysis Value	Design Value	Unit	Analysis/Design
Shear	Vf = 1531	Vr = 2241	lbs	Vf/Vr = 0.68
Moment(+)	Mf = 3010	Mr = 5580	lbs-ft	Mf/Mr = 0.54
Perm. Defl'n	0.07 = <l 999<="" td=""><td>0.45 = L/360</td><td>in</td><td>0.16</td></l>	0.45 = L/360	in	0.16
Live Defl'n	0.18 = L/908	0.45 = L/360	in	0,40
Total Defl'n	0.25 = L/644	0.68 = L/240	in	0,37
Bare Defl'n	0.22 = L/742	0.45 = L/360	in	0.48
Vibration	Lmax = 13'-6	Lv = 18'-0	ft	
Đefl'n	= 0.020	= 0.050	in	0.40

Additional Data:

FACTORS:	f/E	KD	KH	KZ	KL	KT	KS	KN	LC#
Vr	2241	1,00	1.00	-	-	-	-		#2
Mr+	5580	1,00	1.00	-	1.000	-	-	_	#2
EI	253,0	million		-	-	-	-	-	#2

Mr+	5580	1.00	1.00	-	1,000	-	-	_	#2
EI	253,0 m	illion	-	-	-	-	-	-	#2
CRITICAL	LOAD COMB	INATION:	3:						
Shear	: LC #2	= 1.2	5D + 1.5L						

Mo

<pre>foment(+) ;</pre>	LC	#2	=	1.25D + 1.5L	
eflection:	LС	#1	=	1.0D (permanent)	
	LC	#2	=	1.0D + 1.0L (live)	
	LC	#2	=	1.0D + 1.0L (total)	
	TC	# 2		1 OD + 1 OT /bara inight	

LC #2 = 1.0D + 1.0L (total)
LC #2 = 1.0D + 1.0L (bare joist)
Bearing : Support 1 - LC #2 = 1.25D + 1.5L
Support 2 - LC #2 = 1.25D + 1.5L
Load Types: D=dead W=wind S=snow H=earth,groundwater E=earthquake
L=live(use,occupancy) Ls=live(storage,equipment) f=fire
All Load Combinations (LCs) are listed in the Analysis output
CALCULATIONS:
Deflection: ETeff = 318e06 lb-in2 K= 6.18e06 lbs
"Live" deflection = Deflection from all non-dead loads (live, wind, snow...)

Lestgri NOTes:

1. WoodWorks analysis and design are in accordance with the 2010 National Building Code of Canada (NBC Part 4) and the CSA O86-14 Engineering Design in Wood standard (May 2. Please verify that the default deflection limits are appropriate for your application.

3. Refer to technical documentation for installation guidelines and construction details.

4. Nordic I-joists are listed in CCMC evaluation report 13032-R.

5. Joists shall be laterally supported at supports and continuously along the compression edge.

6. The design assumptions and specifications have been provided by the client. Any damages resulting from faulty or incorrect information, specifications, and/or designs furnishels, as their responsibility. This analysis does not constitute a record of the structural integrity of the building nor suitability of the design assumptions made. Nordic Structures is responsible based on the design criteria and loadings shown.

ay 2014 agrifon)



Floor Beam\B19

Dry | 1 span | No cantilevers | 0/12 slope (deg)

BC CALC® Design Report

Build 6536

Job Name: Address:

45147 (5002) Pine Valley

Customer:

City, Province, Postal Code: Vaughan, ON Gold Park

Code reports:

CCMC 12472-R

July 3, 2018 10:33:23

File Name: 290682.bcc

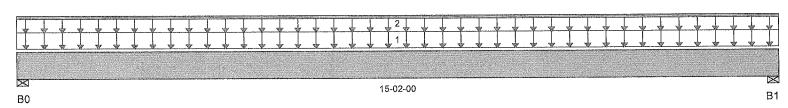
Description: First Floor Framing

Specifier:

Designer: NL

Company: Alpa Roof Trusses

Misc:



Total Horizontal Product Length = 15-02-00

Reaction Summary (Down / Uplift) (lbs)									
Bearing	Live	Dead	Snow	Wind					
B0, 3-1/2"	1,011 / 0	1,034 / 0							
B1, 3-1/2"	1,011 / 0	1,034 / 0							

Load Summary			Live	Dead	Snow Wind	Trib.
Tag Description	Load Type	Ref. Start	End 1.00	0.65	1.00 1.15	
1	Unf. Area (lb/ft^2)	L 00-00-00	15-02-00 40	20		03-04-00
2	Unf, Lin. (lb/ft)	L 00-00-00	15-02-00	60		n/a

	Factored	Factored	Demand /	Load	Location
Controls Summary	Demand	Resistance	Resistance	Case	
Pos. Moment	10,015 ft-lbs	23,220 ft-lbs	43.1%	1	07-07-00
End Shear	2,407 lbs	11,571 lbs	20.8%	1	01-01-00
Total Load Defl.	L/311 (0.568")	0.735"	77.2%	4	07-07-00
Live Load Defl.	L/629 (0.281")	0.49"	57.3%	5	07-07-00
Max Defl.	0.568"	1"	56.8%	4	07-07-00
Span / Depth	18.6	n/a	n/a		00-00-00

Bea	ring Supports	Dim. (L x W)	Demand	Resistance Support	Resistance Member	Material	
B0	Wall/Plate	3-1/2" x 3-1/2"	2,809 lbs	37.3%	18.8%	Spruce Pine	Fir
В1	Wall/Plate	3-1/2" x 3-1/2"	2,809 lbs	37.3%	18.8%	Spruce Pine	Fir

Notes

Design meets Code minimum (L/240) Total load deflection criteria.

Design meets Code minimum (L/360) Live load deflection criteria.

Design meets User specified (1") Maximum Total load deflection criteria.

Calculations assume member is fully braced.

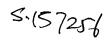
Resistance Factor phi has been applied to all presented results per CSA O86.

BC CALC® analysis is based on Canadian Limit States Design, as per NBCC 2010 and CSA O86.

Design based on Dry Service Condition.

Importance Factor : Normal Part code : Part 4

Nail one ply to another with 3 ½" spiral nails @ (2"



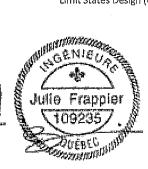


Maximum Floor Spans

Live Load = 40 psf, Dead Load = 15 psf Simple Spans, L/360 Deflection Limit 3/4" OSB G&N Sheathing







			Bai	re			1/2" Gyps	um Ceiling			
Depth	Series	,	On Centre	Spacing		On Centre Spacing					
		1.2"	16"	19.2"	24"	12"	16"	19.2"	24"		
	NI-20	15'-10"	15'-0"	14'-5"	13'-5"	16'-4"	15'-5"	14'-6"	13'-5"		
	NI-40x	17'-0"	16'-0"	15'-5"	14'-9"	17'-5"	16'-5"	15'-10"	15'-2"		
9-1/2"	NI-60	17'-2"	16'-2"	15'-7"	14'-11"	17'-6"	16'-7"	15'-11"	15'-3"		
	NI-70	18'-0"	16'-11"	16'-3"	15'-7"	18'-5"	17'-3"	16'-7"	15'-11"		
	NI-80	18'-3"	17'-1"	16'-5"	15'-9"	18'-8"	17'-5"	16'-9"	16'-1"		
	NI-20	17'-10"	1.6'-10"	16'-2"	15'-6"	18'-6"	17'-4"	16'-9"	16'-1"		
	NI-40x	19'-4"	17'-11"	17'-3"	16'-6"	19'-11"	18'-6"	17'-9"	17'-0"		
44 7/01	NI-60	19'-7"	18'-2"	17'-5"	16'-9"	20'-2"	18'-9"	17'-11"	17'-2"		
11-7/8"	NI-70	20'-9"	. 19'-2"	18'-3"	17'-5"	21'-4"	19'-9"	18'-10"	17'-10"		
	NI-80	21'-1"	19'-5"	18'-6"	17'-7"	21'-7"	20'-0"	19'-0"	18'-0"		
	NI-90x	21'-8"	20'-0"	19'-1"	18'-0"	22'-2"	20'-6"	19'-6"	18'-6"		
	NI-40x	21'-5"	19¹-10"	18'-11"	17'-11"	22'-1"	20'-6"	19'-7"	18'-7"		
	NI-60	21'-10"	20'-2"	19'-3"	18'-2"	22'-5"	20'-10"	19'-11"	18'-10"		
14"	NI-70	23'-0"	21'-3"	20'-3"	19'-2"	23'-8"	21'-11"	20'-10"	19'-9"		
	NI-80	23'-5"	21'-7"	20'-7"	19'-5"	24'-0"	22'-3"	21'-2"	20'-0"		
	NI-90x	24'-1"	22'-3"	21'-2"	20'-0"	24'-8"	22'-10"	21'-9"	20'-7"		
	NI-60	23'-9"	22'-0"	20'-11"	19'-10"	24'-6"	22'-9"	21'-8"	20'-6"		
16"	NI-70	25'-1"	23'-2"	22'-0"	20'-10"	25'-9"	23'-10"	22'-9"	21'-6"		
10	NI-80	25'-6"	23'-6"	22'-4"	21'-2"	26'-1"	24'-2"	23'-1"	21'-10"		
	NI-90x	26'-4"	24'-3"	23'-1"	21'-10"	26'-11"	24'-11"	23'-8"	22'-5"		

			Mid-Spar	n Blocking		Mid-S	Mid-Span Blocking and 1/2" Gypsum Ceiling					
Depth	Series		On Centi	e Spacing			On Centr	e Spacing				
		12"	16"	19.2"	24"	12"	16"	19.2"	24"			
	NI-20	17'-1"	15'-5"	14'-6"	13'-5"	17'-1"	15'-5"	14'-6"	13'-5"			
	NI-40x	18'-8"	17'-6"	16'-7"	15'-3"	19'-2"	1.7'-8"	16'-7"	15'-3"			
9-1/2"	NI-60	18'-11"	17'-8"	16'-10"	15'-7"	19'-4"	18'-0"	16'-10"	15'-7"			
	NI-70	20'-0"	18'-7"	17'-9"	17'-0"	20'-5"	19'-0"	18'-2"	17'-0"			
	NI-80	20'-3"	18'-10"	17'-11"	17'~2"	20'-8"	19'-3"	18'-4"	17'-5"			
	NI-20	20'-2"	18'-8"	17'-6"	16'-2''	20'-7"	18'-8"	17'-6"	16'-2"			
	NI-40x	21'-10"	20'-4"	19'-5"	17'-8"	22'-5"	20'-11"	19'-9"	17'-8"			
44 7/01	NI-60	22'-1"	20'-7"	19'-7"	18'-7"	22'-8"	21'-2"	20'-3"	18'-8"			
11-7/8"	NJ-70	23'-4"	21'-8"	20'-8"	19'-7"	23'-10"	22'-3"	21'-3"	20'-1"			
	NI-80	23'-7"	21'-11"	20'-11"	19'-9"	24'-1"	22'-6"	21.'-5"	20'-4"			
	NI-90x	24'-3"	22'-6"	21'-6"	20'-4"	24'-8"	'23'-0"	22'-0"	20'-9"			
	NI-40x	24'-5"	22'-9"	21'-8"	19'-5"	25'-1"	23'-6"	21'-9"	19'-5"			
	NI-60	24'-10"	23'-1"	22'-0"	20'-10"	25'-6"	23'-10"	22'-9"	21'-4"			
14"	NI-70	26'-1"	24'-3"	23'-2"	21'-10"	26'-8"	24'-11"	23'-9"	22'-6"			
	NI-80	26'-6"	24'-7"	23'-5"	22'-2"	27'-1"	25'-3"	24'-1"	22'-9"			
	NI-90x	27'-3"	25'-4"	24'-1"	22'-9"	27'-9"	25'-11"	24'-8"	23'-4"			
	NI-60	27'-3"	25'-5"	24'-2"	22'-10"	28'-0"	26'-2"	25'-0"	23'-8"			
4.511	NI-70	28'-8"	26'-8"	25'-4"	23'-11"	29'-3"	27'-4"	26'-1"	24'-8"			
16"	NI-80	29'-1"	27'-0"	25'-9"	24'-4"	29'-8"	27'-9"	26'-5"	25'-0"			
	NI-90x	29'-11"	27'-10"	26'-6"	25'-0"	30'-6"	281-5"	27'-2"	25'-8"			

^{1.} Maximum clear span applicable to simple-span residential floor construction with a design live load of 40 psf and dead load of 15 psf. The ultimate limit states are based on the factored loads of 1.50L + 1.25D. The serviceability limit states include the consideration for floor vibration, a live load deflection limit of L/360 and a total load deflection limit of L/240.

^{2.} Spans are based on a composite floor with glued-nailed oriented strand board (OSB) sheathing with a minimum thickness of 3/4 inch for a joist spacing of 24 inches or less. The composite floor may include 1/2 inch gypsum ceiling and/or one row of blocking at mid-span with strapping. Strapping shall be minimum 1x4 inch strap applied to underside of joists at blocking line or 1/2 inch gypsum ceiling attached to joists.

^{3.} Minimum bearing length shall be 1-3/4 inches for the end bearings.

^{4.} Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.

^{5.} This span chart is based on uniform loads. For applications with other than uniformly distributed loads, an engineering analysis may be required based on the use of the design properties. Tables are based on Limit States Design per CSA O86-09, NBC 2010, and OBC 2012.

^{6.} Joists shall be laterally supported at supports and continuously along the compression edge. Refer to technical documentation for installation guidelines and construction details. Nordic I-joists are listed in CCMC evaluation report 13032-R and APA Product Report PR-L274C.



SAFETY AND CONSTRUCTION PRECAUTIONS





Never stack building unsheathed I-joists. Once sheathed, do not over-stress I-laist with concentrated loads from building materials.

WARNING

I-joists are not stable until completely installed, and will not carry any load until fully braced and sheathed.

Avoid Accidents by Following these Important Guidelines:

- Brace and noil each I-joist as it is installed, using hangers, blocking panels, rim board, and/or cross-bridging at joist ends. When I-joists are applied continuous over interior supports and a locad-bening well is planned at that location, blocking will be required at the interior support.
- When the building is completed, the floor sheathing will provide lateral support for the top flanges of the L-jobts. Until this sheathing is applied, temporary bracing, often called struts, or temporary sheathing must be applied to prevent I-joist rollover or buckling.
 - Temporary bracing or stude must be 1x4 inch minimum, at least 8 feet long and spaced no more than 8 feet on centre, and must be secured with a minimum of two 2-1/2? nalls fastened to the top surface of each 1-joist. Nail the bracing to a lateral restraint at the end of each boy. Lop ends of adjoining bracing over at least two 1-joists.
- Or, sheathing (temporary or permanent) can be nailed to the top flange of the first 4 feet of L-joists at the end of the bay.
- 3. For cantilevered L-joists, brace top and bottom flanges, and brace ends with closure panels, rim board, or cross-bridging,
- Install and fully nail permanent sheathing to each t-joist before placing loads on the floor system. Then, stack building materials over beams or walls only.
- 5. Never install a damaged I-joist.

Improper storage or installation, failure to follow applicable building codes, failure to follow span ratings for Nordic Ljoists, failure to failow allowable hole sizes and locations, or failure to use web stifteners when required can result in serious accidents. Follow these installation guidelines carefully.

STORAGE AND HANDLING GUIDELINES

- 1. Bundle wrap can be slippery when wet. Avoid walking an wrapped
- 2. Store, stack, and handle 1-joists vertically and level only.
- 3. Always stack and handle I-joists in the upright position only.
- 4. Do not store I-joists in direct contact with the ground and/or flatwise.
- Protect I-joists from weather, and use spacers to separate bundles. 6. Bundled units should be kept intact until time of installation.
- When handling 1-joists with a crane on the job site, take a few simple precautions to prevent damage to the 1-joists and injury to your work crew.
 - Pick I-joists in bundles as shipped by the supplier.
 - Orient the bundles so that the webs of the I-joists are vertical,
 - Pick the bundles at the 5th points, using a spreader bar if necessary
- 9. NEVER USE OR TRY TO REPAIR A DAMAGED I-JOIST.









INSTALLING NORDIC I-JOISTS

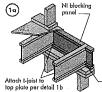
- 1. Before Laying out floor system components, varify that I-joist flange widths match hanger widths. If not, components
- 2. Except for cutting to length, I-joist flonges should never be cut, drilled, or notched.
- 3. Install I-joists so that top and bottom flanges are within 1/2 inch of true vertical alignment.
- I-joists must be anchored securely to supports before floor sheathing is attached, and supports be level.
- ъв leves.

 5. Minimum bearing lengths: 1-3/4 inches for end bearings and 3-1/2 inches for intermediate bearings.
- 6. When using hangers, seat I-joists firmly in hanger bottoms to minimize settlement.
- 7. Leave a 1/16-inch gap between the l-joist end and a header.
- 8. Concentrated loads greater than those that can normally be expected in residential construction should only be applied to the top surface of the top flange. Normal concentrated loads include track lighting fixtures, audio equipment and security cameras. Never suspend unusual or heavy loads from the Lipids's bottom flange. Whenever possible, suspend all concentrated loads from the top of the Lipids. Or, attach the load to blocking that has been securely fastened to the
- 9. Never install I-joists where they will be permanently exposed to weather, or where they will remain in direct contact with
- 10. Restrain ends of floor joists to prevent rollover. Use rim board, rim joists or 1-joist blocking panels.
- 11. For I-joists installed over and beneath bearing walls, use full depth blocking panels, rim board, or squash blocks (cripple members) to transfer gravity loads through the floor system to the wall or foundation below.
- 12. Due to shrinkage, common framing lumber set on odge may never be used as blocking or rim boards. I-joist blocking panels or offise anglineered wood products such as rim board must be cut to fit between the I-joists, and an I-joist-compatible depth selected.
- 13. Provide parmanent lateral support of the bottom flange of all I-joists at Interior supports of multiple-span joists. Similarly, support the bottom flange of all conflavered I-joists at the end support next to the cantilever extension. In the completed structure, the apysour walloard ceiling provides this lateral support. Until the final finished ceiling is applied, temporary bracing or struts must be used.
- 14. If square-edge panels are used, edges must be supported between I-joists with 2x4 blocking. Glue panels to blocking to minimize squeeks. Blocking is not required under structural finish flooring, such as wood strip flooring, or if a separate underlayment layer is installed.
- 15. Nail spacing: Space nails installed to the flange's top face in accordance with the applicable building code requirements or approved building plans.

FIGURE 1
TYPICAL NORDIC 1-JOIST FLOOR FRAMING AND CONSTRUCTION DETAILS

Figures 3, 4 or 5 Some framing requirements such as erection bracing and blacking panels have been omitted for clarity. Holes may be cut in wel for plumbing, wiring on duct work. See Tables 1, and Figure 7. (1d) (1e) NOTE: Never cut or notch flanges. Nordic Lam or Structural or Struction Composite Lumber (SCL) (1b) (1c) Figures 3, -⑽ (1p) 11 (h) (l) (lk) (lm) (10) (11)

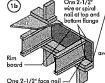
All nalls shown in the above details are assumed to be common wire nails unless otherwise noted. 3' (0.122' dia.) common spiral nails may be substituted for 2-1/2' (0.128' dia.) common wire nails. Framing tumber assumed to be Spruce-Pine-Fir No. 2 or better. Individual components not shown to scale for clarity



2-1/2" nails at 2-1/2" nails at
6" o.c. to top
plate (when used
for lateral shear
transfer, nail to
bearing plate
with same nailing
as required for
decking)

Blocking Panel or Rim Joist	Maximum Factored Uniform Vertical Load* (plf)								
NI Joists	3,300								

"The uniform vertical load is limited to a lost depth of 16 inches or less and is based on standard term load duration it shall not be used in the design of a bending member, such as lots, header, or rafter. For concentrated vertical load transfer, see detail 1d.



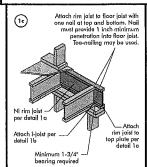
1-1/8" Rim Board Plus

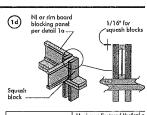
-Attach rim board to top plate using 2-1/2" wire or spiral toe-nails at 6" o.c.

To avoid splitting flange, start nails at least 1-1/2" from end of I-joist. Nails may be driven at an angle to iid splitting of bearing plate.

Minimum bearing length shall be 1-3/4" for the end bearings, and 3-1/2" for the intermediate bearings when applicable. One 2-1/2" face nail — at each side at bearing Blocking Panel or Rim Joist Maximum Factored Uniform Vertical Load* (plf)

8,090 The uniform vertical load is limited to a rim board depth of 16 inches or less and is based on standard term load duration. It shall not be used in the design of a banding member, such as jolst, haoder, or rafter. For concentrated vertical load transfer, see detail 1 d.





Pair of Squash Blocks	Maximum Factored Vertical Pair of Squash Blocks (lbs					
	3-1/2" wide	5-1/2" wid				
2x Lumber	5,500	8,500				
1-1/8" Rim Board Plus	4,300	6,600				

Provide lateral bracing per detail 1a, 1b, or 1c



www.nordicewp.com

lefer to the Installation Guide for Residential Floors for additional information. CCMC EVALUATION REPORT 13032-R

N1-80 NI-90 NI-90x 31/2" | | 1-1/2" | |3.1/2"| |1-1<u>/2"|</u> |8.1/2"| 0SB ₹16"→ ← NI-60 CCFESSION? 3.1/2 NI-40x 1-12-17-1 OSB 3/8"-----OSB 716* OSB 3/6* NI-20 OSB 3/6 ... OSB 3/8 a frappiér 100108717 FSC 2100f MSR 5-P-F No.2 1950f MSR 1950f MSR 2100f MSR 2400f MSR NPG Lumber 33 oieces 33 nieces 33 piece 23 piece 23 pieces 23 pieces

WEB HOLE SPECIFICATIONS

RULES FOR CUTTING HOLES AND DUCT CHASE OPENINGS:

- 1. The distance between the inside edge of the support and the centreline of any hale or duct chase opening shall be in compliance with the requirements of
- 1-joist top and bottom flanges must NEVER be cut, notched, or otherwise madified. Whenever possible, field-cut holes should be centred on the middle of the web.
 The maximum size hole or the maximum depth of a duct chase opening that
- can be cut into an I-joist web shall equal the clear distance between the flanges of the I-joist minus 1/4 inch. A minimum of 1/8 inch should always be maintained between the top or bottom of the hole or opening and the adjacent 1-joist flange.
- 5. The sides of square holes or longest sides of rectangular holes should not exceed 3/4 of
- the diameter of the maximum round hole permitted at that location.

 Where more than one hole is necessary, the distance between adjacent hole edges shall exceed twice the diameter of the largest round hole or twice the size of the largest square hole (or twice the length of the langest side of the langest rectangular hole or duct chase opening) and each hole and duct chase opening shall be sized and located in compliance with the requirements of Tables 1 and 2, respectively.
- A knockout is not considered a hole, may be utilized anywhere it occurs, and may be ignored for purposes of calculating minimum distances between holes and/or duct chase openings.
- 8. Holes measuring 1-1/2 inches or smaller are permitted anywhere in a cantilevered section of a joist. Holes of greater size may be permitted subject to verification.
- 9. A 1-1/2 inch hole or smaller can be placed anywhere in the we provided that it meets the requirements of rule number 6 abov 10. All holes and duct chase openings shall be cut in a workman-li
- manner in accordance with the restrictions listed above and as illustrated in Figure 7.
- 11. Limit three maximum size hales per span, of which one may b a duct chase opening.
- 12. A group of round holes at approximately the same location shall be permitted if they meet the requirements for a single round hole circumscribed around them.

LOCATION OF CIRCULAR HOLES IN JOIST WEBS

Simple or Multiple Span for Dead Loads up to 15 psf and Live Loads up to 40 psf

1.2.1		L	N	linimun	ı Distar	ice fron	n Insid	e Face	of Any	Support	to Cer	ntre of	Hale (ft -	· in.}		
Joist Depth	Joist Series						Rou	nd Hole) Diam	eter (in.)					
		2	3	4	5	6	6-1/4	7	8	8-5/8	9	10	10-3/4	11	12	12-3/4
	NI-20	0'-7"	1'-6"	2'-10"	41-3"	5'-8"	6'-0"			•••						
	NI-40x	0'-7"	1'-6"	3'-0"	4'-4"	6'-0"	6'-4"									
9-1/2"	NI-60	1'-3"	2'-6"	4'-0"	5'-4"	7'-0"	7'-5"									
	NI-70	2'-0"	3'-4"	41-9"	6'-3"	81-011	8'-4"									
	NI-80	2'-3"	3'-6"	5'-0"	6'-6"	8'-2"	8'-8'									
4.2	NI-20	0'-7"	0'-8"	"0-יו	2'-4"	31-8"	4'-0"	51-0"	6'-6"	7'-9"						
	NI-40x	0'-7"	0'-8"	1'-3"	2'-8"	4'-0"	4-4"	5'-5"	7'-0"	8'-4"			***			•••
	NI-60	0'-7"	1'-8"	3'-0"	4'-3"	5'-9"	6'-0"	7'-3"	8'-10"	10'-0"						
11-7/8"	NI-70	1'-3"	2'-6"	4'-0"	5'-4"	6'-9"	7'-2"	8'-4"		. 11'-2"						
ં કે કહ્યું	NI-80	1'-6"	2'-10"	4'-2"	5'-6"	7'-0"	7'-5"	8'-6"	10'-3"							
5.2	NI-90	0'-7"	0'-8"	1'-5"	31-21	4'-10"	5'-4"	6-9	8'-9"	10'-2"						
	NI-90x	0'-7"	0'-8"	0'-9"	2'-5"	4'-4"	4'-9"	6'-3"			`					
i 10	NI-40x	0'-7"	0'-8"	0'-8"	1'-0"	2'-4"	2'-9"	3'-9"	5'-2"	6'-0"	6'-6"	81-36	10'-2"			
	NI-60	0'-7"	0'-8"	1'-8"	3'-0"	4'-3"	4'-8"	5'-8"	7'-2" .	81-01	81-8"	10'-4"	11'-9"	***		***
14"	NI-70	0'-8"	1'-10"	3'-0"	4'-5"	5'-10"	6'-2"	7'-3"	8'-9"	9'-9"	10'-4"	12'-0"	13'-5"			
	NI-80	0'-10"	2'-0"	3'-4"	4'-9"	6'-2"	6'-5"	7'-6"	9'-0"	10'-0"	10'-8"		13'-9"			
40.50	NI-90	0'-7"	0'-8"	0'-10"	2'-5"	4'-0"	4'-5"	5'-9"	7'-5"	8'-8"	91-4"	11'-4"	12'-11"			
	NI-90x	0'-7"	0'-8"	0'-8"	2'-0"	3'-9"	4'-2"	5'-5"	7'-3"	8'-5"	9'-2"					
	N1-60	0'-7"	0'-8"	0'-8"	1'-6"	2'-10"	3'-2"	4'-2"	5'-6"	6'-4"	7'-0°	8'-5"	9'-8"	10'-2"	12'-2"	13'-9"
100	NI-70	0'-7"	1'-0"	2'-3"	3'-6"	4'-10"	5'-3"	6'-3"	7'-8"	8'-6"	9'-2"	10'-8"	12'-0"		14'-0"	15'-6"
16"	NJ-80	0'-7"	1'-3"	2-6"	3'-10"	5'-3"	5'-6"	6'-6"	8'-0"	9'-0"	9'-5"	11'-0"	12'-3"		14'-5"	16'-0"
	NI-90	01-7*	0'-8"	0'-8"	1'-9"	3'-3"	3'-8"	41-9"	6'-5"	7'-5"	8'-0"	9'-10"	11'-3"		13'-9"	15'-4"
	NI-90x	0'-7"	0'-8"	0'-9"	2'-0"	31-6"	4'-0"	5'-0"	6'-9"	7'-9"	8'-4"	10'-2"	11'-6"	12'-0"		

- Above table may be used for I-joist spacing of 24 inches on centre or less.
 Hole location distance is measured from inside face of supports to centre of hole.
 Distances in this chart are based on uniformly loaded joists.
 The above table is based on the I-joists being used at their maximum spans. The minimum distance as given above may be reduced
- for shorter spans; contact your local distributor.

TABLE 2

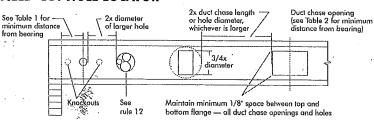
DUCT CHASE OPENING SIZES AND LOCATIONS

Simple Span Only

1.1.		Minim	um distan	ice from in	side face	of suppo	orts to ce	entre of	pening (ft - in.)
Joist Depth	Joist Series		-		Duct Ch	ase Leng	th (in.)			
	55,152	8	10	12	14	16	18	20	22	24
	NJ-20	4'-1"	4'-5"	4'-10"	5'-4"	5'-8"	6'-1"	6'-6"	7'-1"	7'-5"
	NI-40x	5'-3"	5'-8"	6'-0"	6'-5"	6'-10⁵	7'-3"	7'-8"	8'-2"	8'-6"
9-1/2"	NI-60	5'-4"	51-9"	6'-2"	6'-7"	7'-1"	7'-5"	8'-0"	8'-3"	8'-9"
	NI-70	5'-1"	5'-5"	5'-10"	6'-3"	6'-7"	7'-1"	7'-6"	8'-1"	8'-4"
	NI-80	5'-3"	5'-8"	6'-0"	6'-5"	6'-10°	7'-3"	7'-8"	8'-2"	8'-6"
	NI-20	5'-9"	6'-2"	6'-6"	7'-1"	7'-5"	7'-9"	8'-3"	8'-9"	9'-4"
	NI-40x	6'-8"	7'-2"	7'-6"	8'-1"	8'-6"	91-14	9'-6"	10-1"	10'-9"
	NI-60	7'-3"	71-8#	8'-0"	81-61	9'-0"	91-3"	9'-9"	10'-3"	11'-0"
11-7/8"	NI-70	7'-1"	7'-4"	7'-9"	81-31	8'-7"	9'-1"	9'-6"	10'-1"	10'-4"
	NI-80	7'-2"	7'-7"	8'-0"	8'-5"	8'-10"	91-3"	9'-8"	10'-2"	10'-8"
	NI-90	7'-6"	7'-11"	8'-4"	8'-9"	9'-2"	91-7"	10'-1"	10'-7"	10'-11
	NI-90x	7'-7"	' 8'-1"	8'-5"	8'-10"	9'-4"	9'-8"	10'-2"	10'-8"	11'-2"
	NI-40x	8'-1"	8'-7*	91-0=	9'-6"	10'-1"	10'-7"	11'-2"	12'-0"	12'-8"
	NI-60	8'-9"	9'-3"	9'-8"	10'-1"	10'-6"	11'-1"	11'-6"	13'-3"	13'-0"
14"	NI-70	8'-7"	9'-1"	9'-5"	9'-10"	10'-4"	10'-8"	11'-2"	11'-7"	12'-3"
14	NI-80	9'-0"	9'-3"	9'-9"	10'-1"	10'-7"	11'-1"	11'-6"	12'-1"	12'-6"
	NI-90	9'-2"	9'-8"	10'-0"	10'-6"	10'-11'	11'-5"	11'-9"	12'-4"	12'-11
	NI-90x	9'-4"	9'-9"	10'-3"	10'-7"	11'-1"	11'-7"	12'-1"	12'-7"	13'-2"
	NI-60	10'-3"	10'-8"	11'-2"	11'-6"	12'-1"	12'-6"	13'-2"	14'-1"	14'-10
	NI-70	10'-1"	10'-5"	11'-0"	11'-4"	11'-10'	12'-3"	12'-8"	13'-3"	14'-0"
16"	NI-80	10'-4"	10'-9"	11'-3"	11'-9"	12'-1"	12'-7"	13'-1"	13'-8"	14'-4"
	NI-90	10'-9"	11'-2"	11'-8"	12'-0"	12'-6"	13'-0"	13'-6"	14'-2"	14'-10
	NI-90x	ו-יון"	111-5"	11410"	12'-4"	12'-10'	13'-2"	13'-9"	14'-4"	15'-2"

- Above toble may be used for t-joist spacing of 24 inches on centre or less.
 Duct chose opening location distance is measured from inside face of supports to centre of opening.
 The above table is based on simple-span joists only. For other applications, contact your local distribute.
 Distances are based on uniformly loaded floor joists that meet the span requirements for a design li load of 40 psf and dead load of 15 psf, and a live load deflection limit of L/480.
 The above table is based on the l-joists being used at their maximum spans. The minimum distance given above may be reduced for shorter spans; contact your local distributor.

FIELD-CUT HOLE LOCATOR





Knockouts are prescored holes provided for the contractor's convenience to install electrical or small plumbing lines. They are 1-1/2 inches in diameter, and are spaced 15 inches on centre along the length of the I-joist. Where possible, it is preferable to use knockouts instead of field-cut holes.

Never drill, cut or notch the flange, or over-cut the web.

Holes in webs should be cut with a sharp saw.

For rectangular holes, avoid over-cutting the corners, as this can cause unnecessary stress concentrations. Slightly rounding the corners is recommended. Starting the rectangular hole by drilling a 1-inch diameter ho in each of the four corners and then making the cuts b another good method to minimize damage to the 1-joist.

SAFETY AND CONSTRUCTION PRECAUTIONS



fully fastened and braced, or



Never stack building materials over unsheathed I-jaists. Once sheathed, do not over-stress 1-joists with concentrated loads from building materials.

WARNING: I-joists are not stable until completely installed, and will not carry any load until fully braced and sheathed.

AVOID ACCIDENTS BY FOLLOWING THESE IMPORTANT GUIDELINES:

- Brace and noil each I-joist as it is installed, using hangers, blocking panels, rim board, and/or cross-bridging at joist ends.
 When I-joists are applied continuous over interior supports and a load-bearing wall is planned at that location, blocking will required at the interior support.
- When the building is completed, the floor sheathing will provide lateral support for the top flanges of the I-joists. Until this
 sheathing is applied, temporary bracing, often called struts, or temporary sheathing must be applied to prevent I-joist rollover
 or buckling.
 - Temporary bracing or struts must be 1x4 inch minimum, at least 8 feet long and spaced no more than 8 feet on centre, and must be secured with a minimum of two 2-1/2* nails fastened to the top surface of each I-joist. Nail the bracing to a lateral restraint at the end of each bay. Lap ends of adjoining bracing over at least two I-joists.
- Or, sheathing (temporary or permanent) can be nailed to the top flange of the first 4 feet of 1-joists at the end of the bay. 3. For cantilevered 1-joists, brace top and bottom flanges, and brace ends with closure panels, rim board, or cross-bridging.
- 4. Install and fully nail permanent sheathing to each I-joist before placing loads on the floor system. Then, stack building materials over beams or walls only.
- 5. Never install a damaged I-joist.

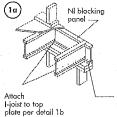
Improper storage or installation, failure to follow applicable building codes, failure to follow span ratings for Nordic I-joists, failure to follow allowable hale sizes and locations, or failure to use web stiffeners when required can result in serious accidents. Follow these installation guidelines carefully.



PRODUCT WARRANTY

Chantiers Chibaugaman guarantees that, in accordance with our specifications, Nordic products are free from manufacturing defects in material and workmanship

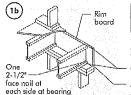
Furthermore, Chantiers Chibougamau warrants that our products, when utilized in accordance with our handling and installation instructions, will meet or exceed our specifications for the lifetime of the structure.



ĺ	Blocking Panel	Maximum Factored Uniform
	or Rim Joist	Yertical Load* (plf)
	NI Joists	3,300

The uniform vertical load is limited to a joist depth of 16 inches or less and is based on standard term load duration. It shall not be used in the design of a bending member, such as joist, header, or rafter. For concentrated vertical load transfer, see detail 1d.

 $2\text{-}1/2^{\rm o}$ nails at 6° o.c. to top plate (when used for lateral shear transfer, nail to bearing plate with same nailing as required for decking)



Blocking Panel	Maximum Factored Uniform
or Rim Joist	Vertical Load* (plf)
1-1/8" Rim Board Plus	8,090

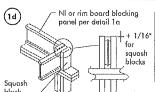
The uniform vertical load is limited to a rim board depth of 16 inches or less and is based on standard term load duration. It shall not be used in the design of a bending member, such as joist, header, or rafter. For concentrated vertical load transfer, see detail 1d.

One 2-1/2" wire or spiral nail at top and bottom flange

Attach rim board to top plate using 2-1/2" wire or spiral toe-nails at 6" o.c.

To avoid splitting flange, start nails at least $1-1/2^\circ$ from end of I-joist. Nails may be driven at an angle to avoid splitting of bearing plate.

Minimum bearing length shall be 1-3/4" for the end bearings, and 3-1/2" for the intermediate bearings when applicable.

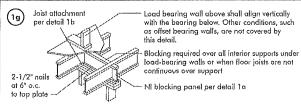


Pair of Squash Blocks	Maximum Factored Vertical Load per Pair of Squash Blocks (lbs)					
	3-1/2" wide	5-1/2" wide				
2x Lumber	5,500	8,500				
1-1/8" Rim Board Plus	4,300	6,600				

Provide lateral bracing per detail 1a or 1b



Transfer load from above to bearing below Install squash blocks per detail 1d. Match bearing area of blocks below to post



Backer block (use if hanger load exceeds 360 lbs). Before installing a backer block to a double I-joist, drive three additional 3° nails through the webs and filler block where the backer block will fit. Clinch. Install backer tight to top flange. Use twelve 3" nails, clinched when possible. Maximum factored resistance for hanger for this detail = 1,620 lbs.

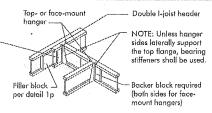
BACKER BLOCKS (Blocks must be long enough to permit required nailing without splitting)

Flange Width	Material Thickness Required*	Minimum Depth**
2-1/2"	l"	5-1/2"
3-1/2"	1-1/2"	7-1/4"

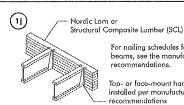
* Minimum grade for backer block material shall be S-P-F No. 2 or better for solid sawn lumber and wood structural panels conforming to CAN/CSA-O325 or CAN/CSA-O437 Standard.

** For face-mount hangers use net joist depth minus 3-1/4" for joists with 1-1/2" thick flanges.

For 2" thick flanges use net depth minus 4-1/4".



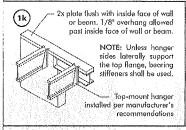
For hanger capacity see hanger manufacturer's recommendations. Verify double 1-joist capacity to support concentrated loads.

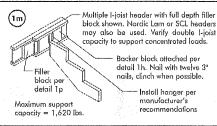


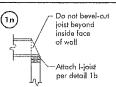
For nailing schedules for multiple beams, see the manufacturer's recommendations.

Top- or face-mount hanger installed per manufacturer's recommendations

NOTE: Unless hanger sides laterally support the top flange, bearing stiffeners shall be used.

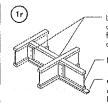






NOTE: Blacking required at bearing for lateral support, not shown for clarity.

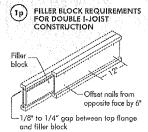
Filler



Lumber 2x4 min., extend block to face of adjacent web. Two 2-1/2" spiral nails from each web to lumber piece, alternate on opposite side.

NI blocking panel

OPTIONAL: Minimum 1x4 inch strap applied to underside of joist at blocking line or 1/2 inch minimum gypsum ceiling attached to underside of joists.

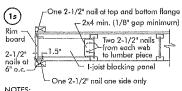


NOTES:

- 1. Support back of I-joist web during nailing to prevent damage to web/flange connection.
- Leave a 1/8 to 1/4-inch gap between top of filler block and bottom of top I-joist flange.
- 3. Filler block is required between joists for full length of span.
- 4. Nail joists together with two rows of 3" nails at 12 inches oc. (clinched when possible) on each side of the double l-joist. Total of four nails per foot required. If nails can be clinched, only two nails per foot are required.
- The maximum factored load that may be applied to one side of the double joist using this detail is 860 lbf/ft. Verify double I-joist capacity.

Size	Depth	Block Size
2-1/2" x 1-1/2"	9-1/2" 11-7/8" 14" 16"	2-1/8" x 6" 2-1/8" x 8" 2-1/8" x 10" 2-1/8" x 12"
3-1/2" x 1-1/2"	9-1/2" 11-7/8" 14" 16"	3" × 6" 3" × 8" 3" × 10" 3" × 12"
3-1/2"× 2"	11-7/8" 14" 16"	3" x 7" 3" x 9" 3" x 1,1"

Flange Net



OTES: In some local codes, blocking is prescriptively required in the first joist space (or first and second joist space) next to the starter joist. Where required, see local code requirements for spacing of the blocking. All nails are common spiral in this detail.

All nails shown in the above details me above aerais are assumed to be common wire nails unless otherwise noted. 3° (0.122° dia.) common spiral nails may be substituted for 2-1/2° (0.128° dia.) common wire nails.
Framing lumber
assumed to be
Spruce-Pine-Fir No. 2
or better. Individual
components not show
to scale for clarity.

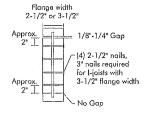
WEB STIFFENERS

RECOMMENDATIONS:

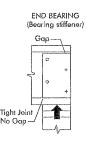
- A bearing stiffener is required in all engineered applications with factored reactions greater than shown in the 1-joist properties table found of the 1-joist Construction Guide (C101). The gap between the stiffener and the flange is at the top
- A bearing stiffener is required when the L-joist is supported in a hanger and the sides of the hanger do not extend up to, and support, the top flange. The gap between the stiffener and flange is at the top.
- A lad stiffener spanished at locations where a factored concentrated load greater than \$2,370 lbs is applied to the top flange between supports or in the case of \$2,370 lbs is applied to the top flange between supports or in the case of \$2,370 lbs is applied to the top flange between the cartilever tip and the support. These values are for standard term load duration, and may be adjusted for other load durations as permitted by the code. The gap between the stiffener and the flange is at the bottom.

FIGURE 2

WEB STIFFENER INSTALLATION DETAILS



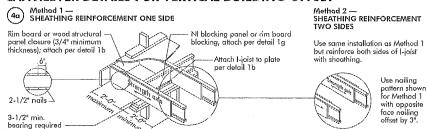
CONCENTRATED LOAD (Load stiffener) Tight Joint-See the adjacent table for web stiffener size requirements



STIFFENER SIZE REQUIREMENTS

Web Stiffener Size Each Side of Web 1" x 2-5/16" minimum width 1-442" x 2-5/16" Confediology width J. FRAPPIER 400400717

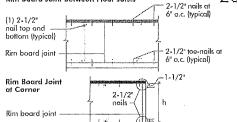
CANTILEVER DETAILS FOR VERTICAL BUILDING OFFSET

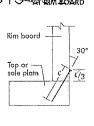


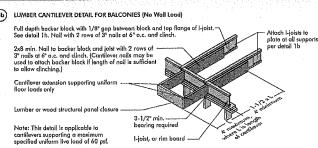
NOTE: Canadian softwood plywood sheathing or equivalent (minimum thickness 3/4") required on sides of joist. Depth shall match the full height of the joist. Nail with 2-1/2" nails at 6" o.c., top and bottom flange. Install with face grain horizontal. Attach I-joist to plate at all supports per detail 1b. Verify reinforced I-joist capacity.

RIM BOARD INSTALLATION DETAILS





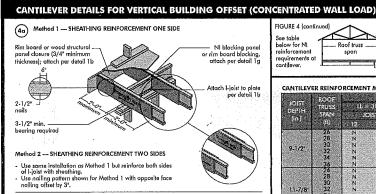




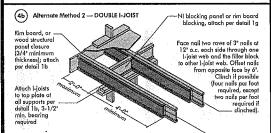
Roof trusses

Girder Roof truss

Span 22-0"



Note: Canadian softwood plywood sheathing or equivalent (minimum thickness 3/4") required on sides of joist. Depth shall match the full height of the joist. Nail with 2-1/2" nails at 6" o.c., top and bottom flange, install with face grain horizontal. Attach I-joist to plate at all supports per detail 1b. Verify reinforced I-joist capacity.



Block I-joists tagether with filler blocks for the full length of the reinforcement. For I-joist flange wildths greater than 3 inches place an additional row of 3° nails along the centreline of the reinforcing panel from each side. Clinch when possible.

FIGURE 4 (continued

	ROOF							UNFAC					
iOlst	10.5	- 10	= 30 msf.	DL = 15	gsf			DL = 15		IL.	= 50 pst	DL = 15	p∗f
хелтн	SPALE		OIST SPA	CING (a	.)	J	CIST SPA	CINGII			OIST SPA	CING (n	1
in)	(6)	12	16	19.2	24	12	16	192	7.4	12	16	19.2	24
	26	N	N	-1	2 X	N		2	Х	N	2	X ···	X X
	28 30 32	N	N	i		N	1	2	X	N	2	X	X
9-1/2'	30	N	1	4	X	N	1	2	X	1	2	×	X X
	32 34	N		2	×	N N	2	X	X		X	X	
	36	N N		· .	X		•		Ŷ	,	û	Ŷ	X X
	72	N	N	Ň	^	Ň	พ		- î	N	N		2
	Ž8	N	N		7.7	N	N	1	2	N	1		x
	26 28 30 32 34	N	N	N	4	N	N ·	i	2	N	1	2	X
11-7/81	32	N.	N	- 1	1	N	N	1	2	N	. 1	2	X
	34	N	N	1	2	N N	1	1	X	N	. 1	2	X X X X
	36	N	N	-1	2	N	100	2	X	N	1	2	X
20 C	36 38 26	N	N	1	2	N		2	<u> </u>	N	2	<u> </u>	Х
	26	N	N	N	N	N	N.	N N		N	N	N	26.0
	28 30	N	N N	N N	N N	N N	N N	N N		N N	N N		
	32	N N	N N	N N		N N	Ñ	N N		N	_ N		
14"	34	N	Ň	N N		N.	N			N	N	•	
		Ň	Ň	N N	4	N	Ň		2	N		1	. 2
	38	N	N	Ň		N	N	1	2	N	1		X
	36 38 40	M	N	N	1	N	N	1	2	N	1	2	X
		1	N	N	N	N	N	N N	N	N.	N	N	- 4
	28	N	N	N	N	N	N	. N	1	N	N	N	- 1
	28 30 32 34	N .	. N	N	74	_ N	N	N	~1 ,,,	- N	N	N .	
	32	N	N	N	N :	- N	N	N .		N	N	. 1	
16"	34	N	N	N	N	N	N N	N N	1	N	N N		- 5
	36	N N	N N	N N		N N	Ň	N		N	- 8		
	38 40 42		N	N N				N		N.	N		
	40	N N	Ñ	N		N	N N		2	N N			2 X

- 1. N = No reinforcement required.
 1 = MI reinforced with 3/4" wood structural
 2 = MI reinforced with 3/4" wood structural
 panel on both sides, or double I-lois.
 X = Try a deeper joist or closer specing.
 2. Maximum design load shall be: 13 pf froof deed load, 55 pf floor total load, and 80 pf well book. Well load is brossed on 3/0" maximum width window or door openings.
- For larger openings, or multiple 3:0° width openings spaced less than 6:0° o.c., additional joints benealth the opening's cripple stude may be required; a cripple stude may be required; a cripple stude may be required; and considered the floor span requirements for a design required to the control of the
- 4. For conventional roof construction using a ridge beam, the Roof Truss Span column obove is equivalent to the distance between the supporting wall and the ridge beam. The root of the r

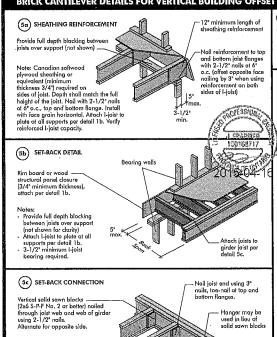
For hip roofs with the lack trusses running parallel to the cantilevered floor joists, the I-joist reinforcement

requirements for a span of 26 ft. shall be permitted to be used.

- 13'-0" maximum

maximum cantilever

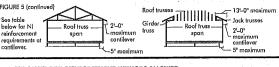
BRICK CANTILEVER DETAILS FOR VERTICAL BUILDING OFFSET (CONCENTRATED WALL LOAD)



Notes:

- Verify girder joist capacity if the back span exceeds the joist spacing.

- Atlach double I-joist per detail 1p, if required.



For hip roofs with the jack trusses running parallel to the cantilevered floor joists, the I-joist reinforcement requirements for a span of 26 ft. shall be permitted to

BRICK CANTILEYER REINFORCEMENT METHODS ALLOWED

	ROOF					KOOFI	OADIN	in Ne	TO PED		400	la visita	
10101	TRUSS	LL :	30 ps/	, DL = 15	pdf -	LL	40 asi	DL = 15	μsf	Щ.	= 50 psf.	$BU = \mathbb{T}$	pd
DEPTH	SPAN	И) ST 59	CINC In		,	OIST SPA	iChiG (n		1	DIST SPA	CING fo)
(0)	(f)	12	16	19.2	24	1,2	16	19.2	24	70	16	19.2	24
	215		X	Υ	Х	2	X	Х	X	- 2	X	X	Х
	26 28 30 32 34	1	X	χ	X	2	X	X	X	X	X	Х.	X
9-1/2"	30	1	X	X	X	2							
	- 32	2	Ŷ	Ŷ	Ŷ	χ̈́	Ŷ	Ŷ	Ŷ	Ŷ	Ŷ	X	Ŷ
- 3	36	2	X	X	X	X	X	X	X_	X	Х	X	X
	26	N	2	Х	λ		. Х	X	X	1	X	X	X
	28	Ŋ	2	Α,	X		X	, A	Ą	2 .	У		- 🗘
11.7/8*	26 28 30 32 34		5	â	Ŷ	1	×	x	Ŷ	2		- û	x
	34	i	Ž.	X	Х	2	X	X	X	2	X	X	X
	36 38	1	X	X	X	2	X	X	Š	X.	X		×
	36	N	, A	X		Ň	- 5		Ŷ	<u> </u>	- 1	x	X
	26 28 30 32 34			χ	×χ		ź	Ŷ	x	i i	X	X	X
	30	N	2	X	. Х	1	2	. Х	. Х	1	X	X	X
14"	32	N	2		X		ž		X		X		, X
		N	- 5	, <u>,</u>	X	ή	Ŷ	^	Ŷ	2	Ŷ	Ŷ	Ŷ
	36 38 40	i i	2	X	X	1 1	X	. X	Х	2	Х.	X	X
	40	1	. Х	Χ	λ	2	X	X	<u> </u>	2	X	X	X
	26 28 30 32 34	N N	1	2	X	N	4	A.	X	N	, ž	`	Ŷ
\$ colon	30		- 1	5	Ŷ	l N	5	â	- x		λ	X	X
	32	N	i	$\tilde{2}$	X	N.	2	X	Х	- 1	Х	Х	X
16"	34	N .	2	X	X		3	X	X	1 1	X	X	X
	1 36	N N	4	, A	Ž	1 4	Q -	A A	Å.	,	×	Ŷ	Ŷ.
	36 38 40 42	N	Ź	x	û	l i	×	x	×	2	X	X	X
	42	1	2	X	X	1	X	χ	X	2		X	

- 1. N = No reinforcement required.
 1 = NI reinforced with 3/4" wood structural panel on one side only.
 2 = NI reinforced with 3/4" wood structural panel on both sides, or double I-joist.
 X = Try a desper joist or close specing.
 2. Moarimum design load shall be XI 5ps proof doad food, 55 psf floor total load, and 80 pff well load. Well load is based on 3-0" maximum width window or door opanings.
- For larger openings, or multiple 3-0" width openings spaced less than 8-0" o.c., additional joils benauth the opening's cripple stud: may be required. Table applies to joils 12 to 24 o.c. that meet the face span requirements for the step less of the student of the step less of the students of the step less of the students of the step less of the students of the step less of the less than the students of the step less of the students into its less of delibertion limit of 1480. Use 12" o.c., requirements for lesser spacing.
- For conventional roof construction using a ridge beam, the Roof Truss Span column obove is equivalent to the distance between the supporting wall and the ridge beam. When the roof is formed using a ridge board, the Roof Truss Span is equivalent to the distance between the supporting walls as if a trus is used.

 Contilewed joint supporting walls as if a roof the roof truss of the roof truss of the roof truss of the roof truss of the roof trusser or roof beams may require additional reinforcing.

RULES FOR CUTTING HOLES AND DUCT CHASE OPENINGS:

- The distance between the inside edge of the support and the centreline of any hole or duct chase opening shall be in compliance with the requirements of Table 1 or 2, respectively.
- 2. I-joist top and bottom flanges must NEVER be cut, notched, or otherwise modified.
- 3. Whenever possible, field-cut holes should be centred on the middle of the web.
- The maximum size hale or the maximum depth of a duct chase opening that can be cut into an Ljoist web shall equal the clear distance between the flanges of the Ljoist minus 1/4 inch. A minimum of 1/8 inch should always be maintained between the top or bottom of the hole or opening and the adjacent Ljoist flange.
- The sides of square holes or longest sides of rectangular holes should not exceed
 3/4 of the diameter of the maximum round hole permitted at that location.
- 3/4 or the Bidmeier or the maximum round note permitted a time tocalient. Where more shan one hole is necessary, the distance between adjacent hole edges shall exceed twice the diameter of the largest round hole or twice the size of the largest square hole for twice the length of the langest side of the langest rectangular hole or duct chase opening and each hale and duct chase apening shall be sized and located in compliance with the requirements of Tables 1 and 2, respectively.
- A knockout is **not** considered a hole, may be utilized anywhere it occurs, and may be ignored for purposes of calculating minimum distances between holes and/or duct chase openings.
- Holes measuring 1-1/2 inches or smaller shall be permitted anywhere in a cantilevered section of a joist, Holes of greater size may be permitted subject to varification.
- A 1-1/2 inch hole or smaller can be placed anywhere in the web provided that it meets the requirements of rule number $6\ above.$
- 10. All holes and duct chase openings shall be cut in a workman-like manner in accordance with the restrictions listed above and as illustrated in Figure 7.
- 11. Limit three maximum size holes per span, of which one may be a duct chase
- A group of round holes at approximately the same location shall be permitted if they meet the requirements for a single round hole circumscribed around them.

TABLE 1 LOCATION OF CIRCULAR HOLES IN JOIST WEBS Simple or Multiple Span for Dead Loads up to 15 psf and Live Loads up to 40 psf

Joist Decili	Joid Series						Ros	nd lic	ye diç	meter (in.)						ndjustme
		2.3	2	-1	5	6	6-174	7	8	8-5/8	9	70	10-3/4	2118	17	12~3/4	Factor
	141-20	0.7	1.6	2-10	4.3	5-8	6'-0'			-	37 mg 213		41.00 may 2		44	÷.	3.6
	NI-40x	G-7°	7-6	3-9	4.4	8-3	84			. Le							14.9
9.1/2"	N8-60	143	7.5	4.0	5'-4"	7-0	7.5	4	•	67.50.00	5 7 3						14.11
	NI-70	2-0		4.0	6-3	8-0	8-4"				200	. ***	100	3100		2.00	19.7
	74-83	2.3	3-6	5.0	8.6	8.2	8-8	-						200			15-9
	NI-20	9-7	0.8	120	2.4	3-8		5-0	6-6"	7.9			-		100	3	5.6
	#8-40x	0.7	7-8	11-31	2.8	4.0	4'-4"	5-5	7-0	8-4	100						
	NI-60	0.7	1.8	347	4:-3"	5.9	6-0*	7-3"	8-10	10-0			100		331303		16.9
11-7/8"	MI-70	1:3	2-6	4.0	54	6'-9"	7-2	8.4	10-0	11.2		12 A C S 12 A					17.5
	14-89	1-6	2-10	4.7	5-6	7.0	7-5	8-6	10-3	114		27.55					17-7
	NI-90	0.7	0'-8'	155	3.2	4-10	5-4	6.9	8.9	10-2		100					17:11
24412044	NI-90s	0.7	0.81	0.9	7-7	4.4	4.9	6.3				2.57 (444) 7.5					18-9
	NI-40x	2.2	9-8	0.8	1.0	2.4	2.9° 408°	3.9	5-2	6.0	9.6	8.3 10.4	10.2		100		17-1
	NI-60	2.7	0.8	11-8	3.0	4.3			7.2	8.0	8-5	7.0					15.2
47	NI-70 NI-80	0.8	7.10	3.0	4.9	9-10 6-2	6'-2' 6'-5'	7.5	7.0	10.0	10.3	32.4	13.5	10.50		-	9.7
	NE-SO	0.7	0.8	0.10	2.5	4.0	0.5	- 9	7.5	8.8	9.4	152	12.11			- 511	19.9
	NI.90.	7.7	0.0	9.8	20	3.9	3.7	3-5	7.3	35	9-2		1000000	70 6 200		66	20-0
	NI-60		0.8	0.8	7.6	2.10	3.5		5.6	6.4	7.5	8.5	9.8	10.5	7.7	13.9	19.10
		9.7			3.6	41.10		4-2	7-8	B-6*	9.2	10-8	17.0	2.4	4.0	51.61	20.10
164	NI-70	9.7	1147	2.3	3.10		5.3	6-3					10.3				
	N-80	0.7	1.3	2.6		5-3	5-6	6.6	847	9.0	9.5	111.0		12.9	14.5	16.0	21.2
	14.90	2.7	0.8	0.8	11,9	3-3	3-81	4.9 5.0	6.5	7.5	8'-0"	9-101		2.0	13-9	15-4	
The state of the s	NI-906	9.7	2-A-1	57.9	7.0	3.5	9.15	2.0	200	7.7	0.4	300 A 100	C 4 80 10 S	1.4.1			4.1

Above table may be used for I-joist specing of 24 inches on centre or less.
 Hale location distance is measured from Inside face of supports to centre of hole
 Distances in this chart are based on uniformly loaded joists.

The above table is based on the 1-joists used at their maximum span. If the 1-joists are placed at less than their full maximum span (see Ma the minimum distance from the centreline of the hole to the face of any support (D) as given above may be reduced as follows:

D_{reduced} = Lactual x D Dreduced =

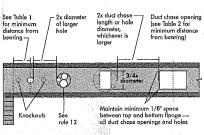
L_{actual} SAF D

Distance from the inside face of any support to centre of hole, reduced for less-than-maximudiatorics shall not be less time 6 inches from the face of the support to edge of the hole. The actual necessived pain sistance between the inside faces of support to (I). Spon Alplatinant Factor given in this table.

The minimum distance from the inside face of ony support to centre of hole from this table. If Section 1, use 1 in the above calculation for Section 1.

ors (1) file And Call 15-54-16

FIGURE 7 FIELD-CUT HOLE LOCATOR



A knockout is NOT considered a hole, may be utilized wherever it occurs and may be ignored for purposes of calculating minimum distances between holes.

Knockouts are prescored holes provided for the contractor's convenience to install electrical or small plumbing lines. They are 1-1/2 inches in diameter, and are spaced 15 inches on centre along the length of the 1-joist. Where possible, it is preferable to use knockouts instead of field-cut holes.



Never drill, cut or notch the flange, or over-cut the web.

The rectangular holes, avoid over-cutling the corners, as this can cause unnecessary stress concentralions. Slightly rounding the corners is recommended. Starting the cratengular hole by drilling a 1-inch diameter hole in each of the four corners and then making the cuts between the holes is another good method to minimize damage to the 1-joist.

TABLE 2
DUCT CHASE OPENING SIZES AND LOCATIONS — Simple Span Only

			an distan	co Irom i	nation for	T. LILE	Trivelia)	sentin i		e (ikita)		
Doella	Josef Serves	Duct chase length (in.)										
Dep.		8	10	12	10	36	18	20	22	24		
	NI-20	4.1	4'.5' 5'.8' 5.9'	4-10	5/-4"	5.8 6.10* 7.1* 6.7* 6.10* 7.5 8.6*	6-1	6'.6" 7-8"	7:-1' 8:2' 8:3'	7-5 8-6 8-4 8-6 9-4 11-0 10-4		
	341-409	5'-3'	5.5	6-0° 6-2°	6-5° 6-7°	5.10	7'-3'	7-8	8.2	3-6		
7-122	NI-60 NI-70	54	5.9	6-2	6-7	7	7.5	8.0	8.3	8.9		
	14-70	5-1	5'-5"	5'-10"	€-3*	and the second	7-3	7-6	8-1: 8-7: 8-9: 10-1: 10-3: 10-1: 10-2:	4.5		
	NI-80	5-3	5-8"	6.0°	6.5 7-1; 8-1; 8-6; 8-3; 8-5; 8-9; 8-10;	8-10	7.3	7.8	5-6	8.6		
Zizar Gilla	NI-20	5'-9'	6.2	0.0	and the second	1300 00 5700		8-3	5-7			
	NI-40x	6'-8' 7'-3'	7-2 7-8	7-6' 8-0' 7-9' 8-0' 8-4 8-5		6-6	9.1° 9.3° 9.1°	9.9°	10-1	0.9		
	M-60	1.1	1.6		0.0	9-0 8-7		y.y	10.5	31.0		
11-7/8	NI-70 NI-80 NI-90 NI-90	7:1*	7:41 7:37 7:11	7.9	5-3	8.7	7-1	9.6	10-1	107 10 44 1		
	NI-052	7.2		6.0	3, 8	8-10	9'-3' 9'-7'	9-8* 10-1*	10.2	10.8		
	1470	7.6		2.4	5.9	9.2	7-7	10-3	10.71	10.11		
0.000	100	7.7	8.1	8-5	P.10	9.4	0,04	10.2	10.00	111.72		
	NI-40x	8-11	8'.7'	9.0 9.8 9.5 9.9	91.6° 101.1° 91.10	10'-1"	10'-7"	111.2	12-0"	10.8 10.11 12.8 13.0 12.3 12.6 12.1 13.0 14.0		
	NI-60	8'-9"	9.3° 9.1° 9.3°	9'-8"	10'-1"	10-6* 10-4* 10-7*	111.11 10.81 111.11 111.5	11.6 11.2 11.6 11.6 11.6 12.1	18.3	1370		
	141-70	8.7	7.1	9.5	9-10	0.0	10.8	1122	4.5	12.3		
	146-80	9.0	9.3	9.9	10	10.7	11.12	11-6	12.1	12'-6'		
	MI-90	9.2	9'.8'	10.0	10'-6"	30.11	11.5	11.9	12.6	12.11		
	N4-90x	9.4	0.8 0.5	10.3	10.7	0.11" 2:1 ₀	11.7	17.1	12.7	33.2		
	16.60	10.3	10-8	11:2	111.6	42-1	12.6	13'-2"	17.15	:4530		
	NI-70	10.1	10.5	11'-0"	114.4	113.10	12.3	12-5	15.3 11.7 12.1 12.4 12.7 12.7 13.7	23 July 19		
10	14.80	10'-4"	10.9	11.3	111.9	1241	121.71		3500 CONTRACT	14'4"		
	NI-90	10.9	1152	111.81	12-0*	12-6	13.0	13'6'	14.2	22 1 45 137		
	M-90x	1100	111.5	31110	12.4	17410	3312	33.91	14'.6	16'.2"		

Above table may be used for I-joilt specing of 24 inches on centre or less.

Duct chase opening location distance is necessived from inside face of supports to contre of opening.

The above table is based on simple-spen losts only, for other applications, contact your local distribution Distances are based on uniformly located float jelds that meat the span requirements for a design live local dead local of 15 gr, and a live local deflection limit of 4280. For either applications, control your local

INSTALLING THE GLUED FLOOR SYSTEM

- 1. Wipe any mud, dirt, water, or ice from I-joist flanges before alvina.
- 2. Snap a chalk line across the I-joists four feet in from the wall for panel edge alignment and as a boundary for spreading glue.
- Spread only enough glue to lay one or two panels at a time, or follow specific recommendations from the glue manufacturer.
- 4. Lay the first panel with tongue side to the wall, and nail in place. This protects the tongue of the next panel from damage when topped into place with a block and sledgehammer.
- 5. Apply a continuous line of glue (about 1/4-inch diameter) to the top flange of a single I-joist. Apply glue in a winding pattern on wide areas, such as with double I-joists.
- 6. Apply two lines of glue on I-joists where panel ends butt to assure proper gluing of each end.
- 7. After the first row of panels is in place, spread glue in the groove of one or two panels at a time before laying the next row. Glue line may be continuous or spaced, but avoid squeeze-out by applying a tilinner line (1/8 lind) than used on 1-joils flanges.
- 8. Tap the second row of panels into place, using a black to protect groove edges.
- Stagger end joints in each succeeding row of panels. A 1/8-inch space between all end joints and
 1/8-inch at all edges, including T&G edges, is recommended. (Use a spacer tool or an 2-1/2" common
 nail to assure accurate and consistent spacing.)
- 10. Complete all nailing of each panel before glue sets. Check the monufacturer's recommendations for cure time. (Warm weather accelerates glue setting), Use 2" ring- or screw-shank noils for panels 3/4-inch thick or less, and 2-1/2" ring- or screw-shank nails for thicker panels. Space nails par the table below. Closer nail spacing may be required by some codes, or for diaphragm construction. The finished deck can be walked on right away and will carry construction loads without damage to the

FASTENERS FOR SHEATHING AND SUBFLOORING(1)

Maximum	Minimum	N	al Size and Ty	Per	Maximum	n Specing) Jenera
Spacing) /	Thickness	Vine or Spired Neels	No.	Skaples	Edges	Interm Supports
16	5/8	2"	1-3/4"	2"	6"	12"
20	5/8	2"	1-3/4"	2*	6"	12*
24	3/4	2"	1-3/4"	2"	6"	12"

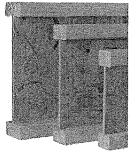
- 1. Fasteners of sheathing and subflooring shall conform to the above table.
- 2. Staples shall not be less than 1/16-inch in diameter or thickness, with not less than a 3/8-inch crown driven with the crown parallel to framing.
- 3. Flooring screws shall not be less than 1/8-inch in diameter.
- 4. Special conditions may impose heavy traffic and concentrated loads that require construction in excess of the minimums shown.
- 5. Use only adhesives conforming to CAN/CGSB-71.26 Standard, Adhesives for Field-Gluing Plywood to Lumber Framing for Floor System, applied in accordance with the manufacturer's recommendations. If OSB panels with sealed surfaces and edges are to be used, use only solvent-based glues; check with panel manufacturer.

Ref.: NRC-CNRC, National Building Code of Canada 2010, Table 9.23.3.5.

IMPORTANT NOTE:
Floor shouthing must be field glued to the 1-joist flanges in order to achieve the maximum spans shown in this document. If sheathing is nalled only, 1-joist spans must be verified with your local distributor.

RIM BOARD INSTALLATION DETAILS (Ba) ATTACHMENT DETAILS WHERE RIM BOARDS ABUT Rim board Joint Between Floor Joists 2-1/2" nails at 6" o.c. (typical) Rim board Joint at Corner 1-1/2 (1) 2-1/2" noil top and bottom (typical) [™]1-1/2" 2-1/2" toe-nails at 6" o.c. (typical) — Rim board loint (8c) 2X LEDGER TO RIM BOARD ATTACHMENT DETAIL (8b) TOE-NAIL CONNECTION AT RIM BOARD Exterior sheathing Remove siding at ledger prior to installation Rim board Floor sheathing Continuous flashing 30° extending at least 3" past Top or sole plate ... joist hange Staggered 1/2" ameler lag screws or thru-bolts with $\ell_{/3}$ diam Deck loist 40.000 S/OV Existing foundation wall - Joist hanger L FRAPPIER 100108717 2x ledger board (preservative-treated); must be greater than or equal to the depth of the deck joist 2015-04-16







MAXIMUM FLOOR SPANS

- Maximum clear spans applicable to simple-span ar multiple-span residential floor construction with a design live load of 40 pst and dead load of 15 pst. The ultimate limit states are based on the factored loads of 1.50t. +
 1.25D. The serviceobility limit states include the consideration for floor vibration and a live load delilection limit of L/480.
 For multiple-span applications, the and spans shall be 40% or more of the adjacent span.
- S miss of the sudjection spain.

 Spans are based on a composite floor with glued-nailed oriented strand board (CSB) shealthing with a minimum lickness of \$50 kinch for joist spacing of \$24 inches. Adhesive less, or \$3/4 inch for joist spacing of \$24 inches. Adhesive shall meet the requirements given in CGBS-71.26 Standard. No concrete topping or bridging element was assumed. Increased spans may be achieved with the used of gyprum and/or a row of blocking at mid-span.
- 3. Minimum bearing length shall be 1-3/4 inches for the end bearings, and 3-1/2 inches for the intermediate bearings.
- Bearing stiffeners are not required when I-joists are used with the spans and spacings given in this table, except as required for hangers.
- This span chart is based on uniform loads. For applications with other than uniform loads, an engineering analysis may be required based on the use of the design properties.
- 6. Tables are based on Limit States Design per CAN/CSA O86-09 Standard, and NBC 2010.
- 7. St units conversion: 1 inch = 25.4 mm 1 foot = 0.305 m

MAXIMUM FLOOR SPANS FOR NORDIC 1-JOISTS

Joie	Joint			Ad application					
10-1011			On centr	Specific	100		On contr		
		42	16	19.2	7/9	125	16	19.2	7/L
300000	NI-20	15'-1'	14'-2'	13'-9"	13'-5'	16'-3"	15'-4°	14'-10"	14'-7'
	NI-40x	16-1*	15'-2"	14'-8"	14'-9"	17'-5"	16-5	15'-10"	15'-5'
9-1/2	NI-60	16.3	15'-4"	74'-10"	14'-11'	17'7'	16'-7"	16'-0"	16'-1"
	NI-70	17-11	16'-1"	15-6	15'-7"	18*-7*	17'-4"	16'-9"	16'-10"
	NI-80	17-3	16'-3'	15'-8"	15'-9"	18-10	17'-6"	16'-11'	17'0"
	NI-20	16-11	16'-0'	15-5	15'-6'	18-4	17'-3'	16'-8°	16'-7'
1	NI-40a	18-1	17'-0"	16'-5"	16'-6"	20'-0"	18-5	17'-9"	17'-7"
	NI-60	18-4"	17'-3"	16'-7"	16'-9"	20-3*	18-91	18-0*	16-1*
11-7/8	NI-70	19-6*	18'-0"	17-4	17'-5"	21'-6"	19'-11'	19'-0"	19'-11
2.2	NI-80	19.9	18'-3"	1756	17-7	211-9*	20'-2'	19:-3*	19'-4"
	NI-90	20'-2'	18-7	17-10	17:11*	22'-3"	20'-7"	19'-8"	17'-9"
THE RESERVE	NI-90+	20'-4'	18-9"	17411	16'-0"	22'-5'	20'-9"	19'-10"	19.114
	N1-404	20'-1'	18-7	17'-10'	17:41:	22.2	20'-6'	19'-8"	19'-4"
	NI-60	20'-5°	18-11*	18-1"	18-2	22'-7"	20'-11"	20'-0"	20'-1"
	NI-70	211.71	20-0*	19-1	19'-2'	23'-70"	22'-1'	21'-1"	2142
74'	NI-80	21'-11'	20'-3'	1904	19'-5'	24'-3'	22'-5'	21'-5"	21'-6'
	NI-90	22'-5'	20'-8'	19-9	19'-10"	24'-9"	22'-10"	21'-10"	21'-10"
	NI-90x	22'-7"	20'-11°	19-11	20'-0"	25'-0"	23'-1"	22'-0"	22'-2"
50.045.00	NI-60	22'-3"	20'-8"	19-9	19-10	24'-7'	22'-9"	21'-9"	21'-10"
	NI-70	23'-6"	21'-9"	20-9	20'-10"	26'-0"	24'-0"	22'-11"	23'-0'
16"	NI-80	23-11	22'-1"	21'-1"	21'-2"	26'-5"	24'-5'	23'-3"	23'-4'
200	NI-90	24'-5"	22'-6"	21'-5'	21'-6'	26'-11'	24'-10"	23'-9"	23'-9"
	NI-90*	24'-8'	221-91	214.94	21'-10"	27-3	25'-2"	24'-0"	24'-1"

CCMC EVALUATION REPORT 13032-R

I-JOIST HANGERS

- 1. Hangers shown illustrate the three to support 1-joists.
- All nailing must meet the hanger manufacturer's recommendations.
- Hangers should be selected based on the joist depth, flange width and load capacity based on the maximum spans.
- 4. Web stiffeners are required when the sides of the hangers do not laterally brace the top flange of the I-joist.







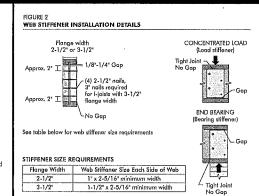
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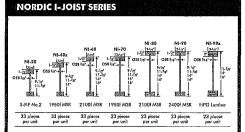
WEB STIFFENERS

RECOMMENDATIONS:

- A bearing stiffener is required in all engineered applications with factored reactions greater than shown in the lipids preparties table found of the Lipids Toperaties table found of the Lipids Toperaties table found of the Lipids Construction Guide (C101). The gap between the stiffener and the flarge is at the top.
- A bearing stiffener is required when the I-joist is supported in a hanger and the sides of the hanger do not extend up to, and support, the top flangs. The gap between the stiffener and flange is at the top.
- A load stiffener is required at locations a Noad stiffener is required at locations where a factored occantroted load greater than 2,370 lbs is applied to the top flange between supports, or in the case of a conflictive, anywhere between supports, or its case of a conflictive, anywhere between the cantilever tip and the support. These values are for standard term load duration, and may be adopted for after load durations as permitted by the code. The gap between the stiffener and the filance is at this between the stiffener. y the code. The gap between t nd the flange is at the bottom.

SI units conversion: 1 inch = 25.4 mm

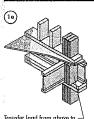




Chantiers Chibougamau Ltd. harvests its own trees, which enables Nozzlic products to adhere to strict quality control procedures through the State manufacturing process. Every phase of the operation, traps of the strict process.

manufacturing process. Every phase of the operation, in this had product, riflects our commitment to qualify.

Nordic Engineered Wood Libits use only finger-jointed back, stypic in the flonges, ensuring consistent quality, superior stypic in the flonges, ensuring consistent quality, superior stypic in the flonger span carrying capacity.



insfer load from above to

1

Use single I-joist for loads up to 3,300 plf, double I-joists for loads up to 6,600 plf (filler block not required). Altach I-joist to (1f) top plate using 2-1/2" nails Provide backer for siding attachment unless nailable sheathing is used. Wall sheathing, as required ---

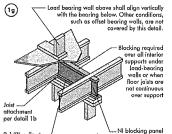
Rim board may be used in lieu of I-joists. Backer is not required when rim board is used. Bracing per code shall be carried to the foundation.

2x plate flush with inside face of wall or beam. 1/8" overhang

allowed past inside

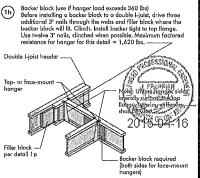
installed on Top-mount hanger installed per ... manufacturer's recommendations

face of wall or beam



NI blocking panel per detall 1a 2-1/2" nails at 6" a.c. to top p

(1n)



For hanger capacity see hanger manufacturer's recommendations. Verify double L-joist capacity to support concentrated loads.

Install hanger per manufacturer's recommendations

(1m)

Filler block per detall 1p ...

Backer block attached per — detail 1h. Nail with twelve 3° nails, clinch when possible.

Multiple I-joist header with full depth filler block shown, Nordic Lam or SCL

headers may also be used. Verify double t-joist capacity to support

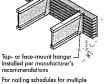
Maximum support capacity = 1,620 lbs.

Note: Blocking required at bearing for lateral support, not shown for clarity.

BACKER BLOCKS (Blocks must be long enough to permit required nailing without splitting)

Flunge Width	Material Thickness Required*	Minimum Depth**
2-1/2"	1"	5-1/2"
3-1/2"	1-1/2"	7-1/4"

Minimum grade for bocker block material shall be S-P.F No, 2 or better for salid sown lumber and wood structural panels conforming to CAN/CSA-0375 or CAN/CSA-



Nordic Lam or SCL

beams, see the manufacturer's recommendations.

Note: Unless hanger sides laterally support the top flange, bearing stiffeners shall be used.

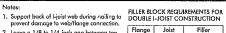
(1k)

Note: Unless hanger sides laterally support the top flange, bearing stiffeners shall be used.

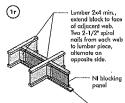
ount hana

- Leave a 1/8 to 1/4-inch gap between top of filler black and bottom of top I-joist flange.
- Not rength at span.

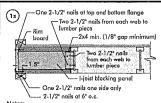
 A. Nail joists togather with two rows of 3° nails at 12 inches a.c. (clinched when possible) on each side of the double 1-joist. Total of four nails per foot required. If nails can be clinched, only two nails per foot are required.
- 5. The maximum factored load that may be applied to one side of the double joist using this detail is 860 lbf/ft. Verify double 1-joist capacity.



Flange Size	Joist Depth	Filler Block Size
2-1/2" x 1-1/2"	9-1/2" 11-7/8" 14" 16"	2-1/8° x 6° 2-1/8" x 8° 2-1/8" x 10° 2-1/8° x 12°
3-1/2" x 1-1/2"	9-1/2" 11-7/8" 14" 16"	3" x 6" 3" x 8" 3" x 10" 3" x 12"
3-1/2" x 2"	11-7/8" 14" 16"	3" x 7" 3" x 9" 3" x 11"

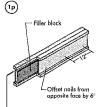


Optional: Minimum 1x4 inch strap applied to underside of joist at blacking line or 1/2 inch minimum gypsum ceiling attached to underside of joists.



Notes:
In some local codes, blocking is prescriptively required in the first joist space (or first and second joist space) next to the starter joist. Where required, see local code requirement for spacing of the blocking.

All nails are common spiral in this detail.



-1/8° to 1/4" gap between top flange and filler block